

Data and Formulae for Mechanical Engineering Students

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A General information

Table A.1: SI Units and abbreviations

Quantity	Unit	Unit symbol
Basic units		
Length	metre	m
Mass	kilogram	kg
Time	second	s
Electric current	ampere	A
Thermodynamic temperature	kelvin	K
Luminous intensity	candela	cd
Derived units		
Acceleration, linear	metre/second ²	m s^{-2}
Acceleration, angular	radian/second ²	rad s^{-2}
Area	metre ²	m^2
Density	kilogram/metre ³	kg m^{-3}
Force	newton	$\text{N} (= \text{kg m s}^{-2})$
Frequency	hertz	$(\text{Hz} = \text{s}^{-1})$
Impulse, linear	newton-second	N s
Impulse, angular	newton-metre-second	N m s
Moment of force	newton-metre	N m
Second moment of area	metre ⁴	m^4
Moment of inertia	kilogram-metre ²	kg m^2
Momentum, linear	kilogram-metre/second	kg m s^{-1}
Momentum, angular	kilogram-metre ² /second	$\text{kg m}^2 \text{s}^{-1}$
Power	watt	$\text{W} (= \text{J s}^{-1} = \text{N m s}^{-1})$
Pressure, stress	pascal	$\text{Pa} (= \text{N m}^{-2})$
Stiffness (linear), spring constant	newton/metre	N m^{-1}
Velocity, linear	metre/second	m s^{-1}
Velocity, angular	radian/second	rad s^{-1}
Volume	metre ³	m^3
Work, energy	joule	$\text{J} (= \text{N m})$
Electrical units		
Potential	volt	$\text{V} (= \text{W A}^{-1})$
Resistance	ohm	$\Omega (= \text{V A}^{-1})$
Charge	coulomb	$\text{C} (= \text{A s})$
Capacitance	farad	$\text{F} (= \text{A s V}^{-1})$
Electric field strength	volt/metre	V m^{-1}
Electric flux density	coulomb/metre ²	C m^{-2}
Magnetic units		
Magnetic flux	weber	$\text{Wb} (= \text{V s})$
Inductance	henry	$\text{H} (= \text{V s A}^{-1})$
Magnetic field strength	—	A m^{-1}
Magnetic flux density	—	Wb m^{-2}

Table A.2: Conversion factors from Imperial to SI units

To convert	from	to	multiply by
Acceleration	foot/second ² (ft/sec ²)	metre/second ² (m s ⁻²)	0.3048
	inch/second ² (in/sec ²)	metre/second ² (m s ⁻²)	0.0254
Area	foot ² (ft ²)	metre ² (m ²)	0.092903
	inch ² (in. ²)	metre ² (m ²)	6.4516×10^{-4}
Density	pound mass/inch ³ (lbm/in ³)	kilogram/metre ³ (kg m ⁻³)	2.7680×10^4
	pound mass/foot ³ (lbm/ft ³)	kilogram/metre ³ (kg m ⁻³)	16.018
Force	kip (1000 lb)	newton (N)	4.4482×10^3
	pound force (lb)	newton (N)	4.4482
Length	foot (ft)	metre (m)	0.3048
	inch (in)	metre (m)	0.0254
	mile (mi), U.S. statute	metre (m)	1.6093×10^3
	mile (mi), international nautical	metre (m)	1.852×10^3
Mass	pound mass (lbm)	kilogram (kg)	0.45359
	slug (lb-sec ² /ft)	kilogram (kg)	14.594
	ton (2000 lbm)	kilogram (kg)	907.18
Moment of force	pound-foot (lb-ft)	newton-metre (N m)	1.3558
	pound-inch (lb-in.)	newton-metre (N m)	0.11298
Moment of inertia	pound-foot-second ² (lb-ft-sec ²)	kilogram-metre ² (kg m ²)	1.3558
Momentum, linear	pound-second (lb-sec)	kilogram-metre/second (kg m s ⁻¹)	4.4482
Momentum, angular	pound-foot-second (lb-ft-sec)	newton-metre-second (kg m ² s ⁻¹)	1.3558
Power	foot-pound/minute (ft-lb/min)	watt (W)	0.022597
	horsepower (550 ft-lb/sec)	watt (W)	745.70
Pressure, stress	atmosphere (std) (14.7 lb/in ²)	newton/metre ² (N m ⁻² or Pa)	1.0133×10^5
	pound/foot ² (lb/ft ²)	newton/metre ² (N m ⁻² or Pa)	47.880
	pound/inch ² (lb/in. ² or psi)	newton/metre ² (N m ⁻² or Pa)	6.8948×10^3
Second moment of area	inch ⁴	metre ⁴ (m ⁴)	41.623×10^{-8}
Stiffness (linear)	pound/inch (lb/in.)	newton/metre (N m ⁻¹)	175.13
Velocity	foot/second (ft/sec)	metre/second (m s ⁻¹)	0.3048
	knot (nautical mi/hr)	metre/second (m s ⁻¹)	0.51444
	mile/hour (mi/hr)	metre/second (m s ⁻¹)	0.44704
	mile/hour (mi/hr)	kilometre/hour (km h ⁻¹)	1.6093
Volume	foot ³ (ft ³)	metre ³ (m ³)	0.028317
	inch ³ (in. ³)	metre ³ (m ³)	1.6387×10^{-5}
	UK gallon	metre ³ (m ³)	4.546×10^{-3}
Work, Energy	British thermal unit (BTU)	joule (J)	1.0551×10^3
	foot-pound force (ft-lb)	joule (J)	1.3558
	kilowatt-hour (kw-h)	joule (J)	3.60×10^6

Table A.3: Decimal prefixes

Multiplication factor ^a		Prefix	Symbol
1 000 000 000 000	= 10^{12}	tera	T
1 000 000 000	= 10^9	giga	G
1 000 000	= 10^6	mega	M
1 000	= 10^3	kilo	k
100	= 10^2	hecto ^a	h
10	= 10	deka ^a	da
0.1	= 10^{-1}	deci ^b	d
0.01	= 10^{-2}	centi	c
0.001	= 10^{-3}	milli	m
0.000 001	= 10^{-6}	micro	μ
0.000 000 001	= 10^{-9}	nano	n
0.000 000 000 001	= 10^{-12}	pico	p

^aUse prefixes to keep numerical values generally between 0.1 and 1000

^bThe use of prefixes hecto, deka, deci and centi should be avoided except for certain areas or volumes where the numbers would otherwise become awkward.

Table A.4: Physical constants

Avogadro's number ^a	N	$6.022 \times 10^{23} \text{ mol}^{-1}$
Absolute zero of temperature	—	$0 \text{ K} = -273.2^\circ\text{C}$
Boltzmann's constant	k	$1.380 \times 10^{-23} \text{ J K}^{-1}$
Characteristic impedance of vacuum	Z_0	$= \left(\frac{\mu_0}{\epsilon_0} \right)^{1/2} = 120\pi \Omega$
Electron volt	eV	$1.602 \times 10^{-19} \text{ J}$
Electronic charge	e	$1.602 \times 10^{-19} \text{ C}$
Electronic rest mass	m_e	$9.109 \times 10^{-31} \text{ kg}$
Electronic charge to mass ratio	$\left(\frac{e}{m_e} \right)$	$1.759 \times 10^{11} \text{ C kg}^{-1}$
Faraday's constant ^a	F	$9.65 \times 10^4 \text{ C mol}^{-1}$
Gas constant ^a	\bar{R}	$8.314 \text{ J mol}^{-1} \text{ K}^{-1}$
Permeability of free space	μ_0	$4\pi \times 10^{-7} \text{ H m}^{-1}$
Permittivity of free space	ϵ_0	$\frac{1}{36\pi} \times 10^{-9} \text{ F m}^{-1}$
Planck's constant	h	$6.626 \times 10^{-34} \text{ J s}$
Standard gravitational acceleration	g	9.807 m s^{-2}
Stefan-Boltzmann constant	σ	$5.67 \times 10^{-8} \text{ J m}^{-2} \text{ s}^{-1} \text{ K}^{-4}$
Velocity of light in vacuum	c	$2.9979 \times 10^8 \text{ m s}^{-1}$
Volume of perfect gas at S.T.P. ^b	—	$22.42 \times 10^{-3} \text{ m}^3$

^aThese are conventional definitions in gram mol units. For SI calculations in kg mol units multiply the values given by 10^3

^bAt Standard Temperature (0°C) and Pressure (one atmosphere pressure or $1.013 \times 10^5 \text{ N m}^{-2}$)

B Mathematics and computing

Data and formulae for core course examinations in:

- Mathematics
- Computing

and in other, related, optional courses.

B.1 Algebra

B.1.1 Logarithms

If $b^y = x$, $y = \log_b(x)$ and:

$$\log(x_1 x_2) = \log x_1 + \log x_2$$

$$\log\left(\frac{x_1}{x_2}\right) = \log x_1 - \log x_2$$

$$\log\left(\frac{1}{x}\right) = -\log x$$

$$\log x^n = n \log x$$

$$\log 1 = 0$$

For natural logarithms $b = e = 2.718282$ and if $e^y = x$,

$$y = \log_e(x) = \ln(x)$$

Hence

$$\log_{10} x = 0.4343 \ln x.$$

B.1.2 Quadratic equations

If $ax^2 + bx + c = 0$, then

$$x = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a}$$

and ($b^2 > 4ac$) for real roots.

B.1.3 Determinants

2nd order:

$$\begin{vmatrix} a_1 & b_1 \\ a_2 & b_2 \end{vmatrix} = a_1 b_2 - a_2 b_1$$

3rd order:

$$\begin{vmatrix} a_1 & a_2 & a_3 \\ b_1 & b_2 & b_3 \\ c_1 & c_2 & c_3 \end{vmatrix} = +a_1 b_2 c_3 + a_2 b_3 c_1 + a_3 b_1 c_2 - a_3 b_2 c_1 - a_2 b_1 c_3 - a_1 b_3 c_2$$

B.1.4 Vector algebra

$$\mathbf{a} = (a_1 \mathbf{i} + a_2 \mathbf{j} + a_3 \mathbf{k}) = (a_1, a_2, a_3) \text{ etc.}$$

Scalar (dot) product:

$$\mathbf{a} \cdot \mathbf{b} = a_1 b_1 + a_2 b_2 + a_3 b_3$$

Vector (cross) product:

$$\mathbf{a} \times \mathbf{b} = \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ a_1 & a_2 & a_3 \\ b_1 & b_2 & b_3 \end{vmatrix}$$

Scalar triple product:

$$[\mathbf{a}, \mathbf{b}, \mathbf{c}] = \mathbf{a} \cdot \mathbf{b} \times \mathbf{c} = \mathbf{b} \cdot \mathbf{c} \times \mathbf{a} = \mathbf{c} \cdot \mathbf{a} \times \mathbf{b} = \begin{vmatrix} a_1 & a_2 & a_3 \\ b_1 & b_2 & b_3 \\ c_1 & c_2 & c_3 \end{vmatrix}$$

Vector triple product:

$$\mathbf{a} \times (\mathbf{b} \times \mathbf{c}) = \mathbf{b} (\mathbf{a} \cdot \mathbf{c}) - \mathbf{c} (\mathbf{a} \cdot \mathbf{b})$$

B.1.5 Series

Binomial series:

$$(1+x)^\alpha = 1 + \alpha x + \frac{\alpha(\alpha-1)}{2!} x^2 + \frac{\alpha(\alpha-1)(\alpha-2)}{3!} x^3 + \dots \quad (\alpha \text{ arbitrary, } |x| < 1).$$

$$e^x = 1 + x + \frac{x^2}{2!} + \dots + \frac{x^n}{n!} + \dots \quad (|x| < \infty)$$

$$\cos x = 1 - \frac{x^2}{2!} + \frac{x^4}{4!} - \dots + (-1)^n \frac{x^{2n}}{(2n)!} + \dots \quad (|x| < \infty)$$

$$\sin x = x - \frac{x^3}{3!} + \frac{x^5}{5!} - \dots + (-1)^n \frac{x^{2n+1}}{(2n+1)!} + \dots \quad (|x| < \infty)$$

$$\tan x = x + \frac{x^3}{3} + \frac{2x^5}{15} + \frac{17x^7}{315} + \dots \quad \left(-\frac{\pi}{2} < x < \frac{\pi}{2}\right)$$

$$\sinh x = \frac{e^x - e^{-x}}{2} = x + \frac{x^3}{3!} + \frac{x^5}{5!} + \frac{x^7}{7!} + \dots \quad (|x| < \infty)$$

$$\cosh x = \frac{e^x + e^{-x}}{2} = 1 + \frac{x^2}{2!} + \frac{x^4}{4!} + \frac{x^6}{6!} + \dots \quad (|x| < \infty)$$

$$\ln(1+x) = x - \frac{x^2}{2} + \frac{x^3}{3} - \dots + (-1)^n \frac{x^{n+1}}{(n+1)} + \dots \quad (-1 < x < 1)$$

Stirling's formula for $n!$ when n is large:

$$n! \cong \left(\frac{n}{e}\right)^n \sqrt{2\pi n}$$

or

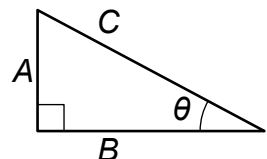
$$\ln(n!) \cong \left(n + \frac{1}{2}\right) \ln n - n + \frac{1}{2} \ln(2\pi)$$

or

$$\log_{10}(n!) \cong 0.39909 + \left(n + \frac{1}{2}\right) \log_{10} n - 0.43429n$$

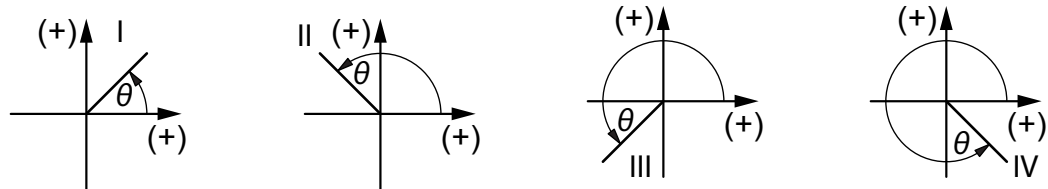
B.1.6 Trigonometry

Definitions:



$$\begin{aligned} \sin \theta &= \frac{A}{C} & \cos \theta &= \frac{B}{C} & \tan \theta &= \frac{A}{B} \\ \csc \theta &= \frac{C}{A} & \sec \theta &= \frac{C}{B} & \cot \theta &= \frac{B}{A} \end{aligned}$$

Signs of trigonometric functions in the four quadrants:



Quadrant:	I	II	III	IV
$\sin \theta$	+	+	-	-
$\cos \theta$	+	-	-	+
$\tan \theta$	+	-	+	-
$\csc \theta$	+	+	-	-
$\sec \theta$	+	-	-	+
$\cot \theta$	+	-	+	-

Trigonometrical identities

$$\cos^2 \theta + \sin^2 \theta = 1$$

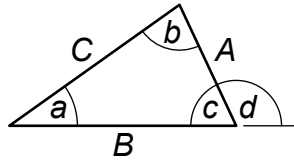
$$1 + \tan^2 \theta = \sec^2 \theta$$

$$\sin 2\theta = 2 \sin \theta \cos \theta$$

$$\cos 2\theta = \cos^2 \theta - \sin^2 \theta = 2 \cos^2 \theta - 1 = 1 - 2 \sin^2 \theta$$

$$\sin \frac{\theta}{2} = \sqrt{\frac{1}{2} (1 - \cos \theta)}$$

$$\cos \frac{\theta}{2} = \sqrt{\frac{1}{2} (1 + \cos \theta)}$$



Sine rule: $\frac{A}{\sin a} = \frac{B}{\sin b} = \frac{C}{\sin c}$

Cosine rule: $C^2 = A^2 + B^2 - 2AB \cos c$
 $C^2 = A^2 + B^2 + 2AB \cos d$

$$\sin(a + b) = \sin a \cos b + \cos a \sin b$$

$$\cos(a + b) = \cos a \cos b - \sin a \sin b$$

$$\sin(a - b) = \sin a \cos b - \cos a \sin b$$

$$\cos(a + b) = \cos a \cos b + \sin a \sin b$$

$$\sin a + \sin b = 2 \sin\left(\frac{a+b}{2}\right) \cos\left(\frac{a-b}{2}\right)$$

$$\cos a + \cos b = 2 \cos\left(\frac{a+b}{2}\right) \cos\left(\frac{a-b}{2}\right)$$

$$\sin a - \sin b = 2 \cos\left(\frac{a+b}{2}\right) \sin\left(\frac{a-b}{2}\right)$$

$$\cos a - \cos b = -2 \sin\left(\frac{a+b}{2}\right) \sin\left(\frac{a-b}{2}\right)$$

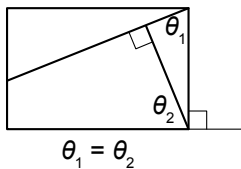
$$\sin iz = i \sinh z$$

$$\cos iz = \cosh z$$

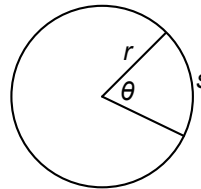
$$\sinh iz = i \sin z$$

$$\cosh iz = \cos z$$

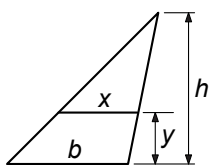
B.1.7 Geometry



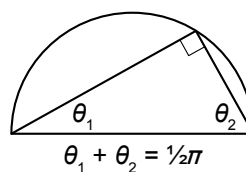
When the two intersecting lines are, respectively, perpendicular to two other lines, the angles formed by each pair are equal.



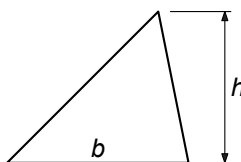
Circle:
 circumference = $2\pi r$
 Arc length $s = r\theta$
 Sector area = $\frac{1}{2}r^2\theta$



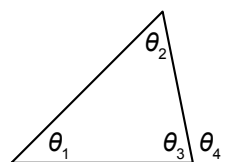
Similar triangles:
 $\frac{x}{b} = \frac{h-y}{h}$



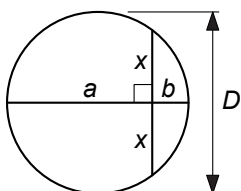
Every triangle inscribed within a semicircle is a right triangle.



Any triangle:
 Area = $\frac{1}{2}bh$

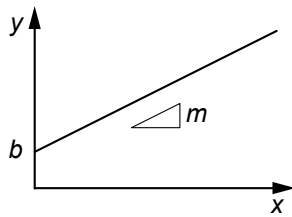


Angles of a triangle:
 $\theta_1 + \theta_2 + \theta_3 = 180^\circ$
 $\theta_4 + \theta_1 + \theta_2$

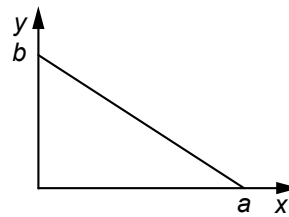


Intersecting chords:
 $x^2 = ab$
 $x^2 \approx Db$ when $b \ll D$

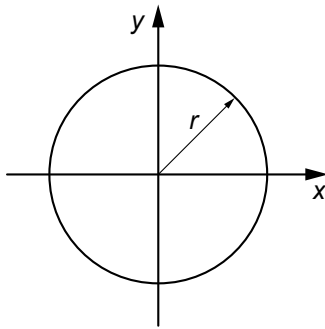
B.1.8 Analytic geometry



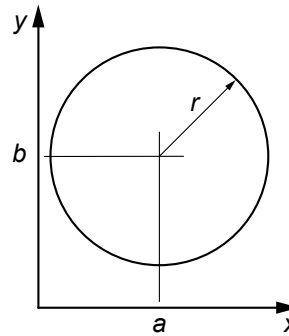
Straight line:
 $y = b + mx$



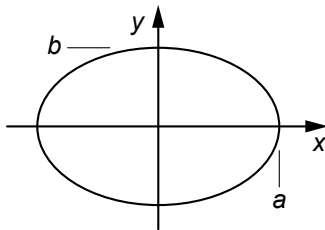
$$\frac{x}{a} + \frac{y}{b} = 1$$



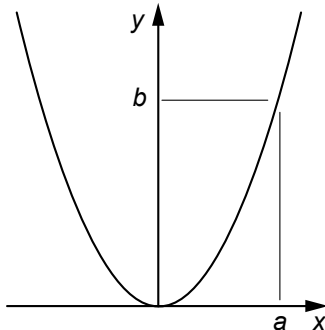
Circle:
 $x^2 + y^2 = r^2$



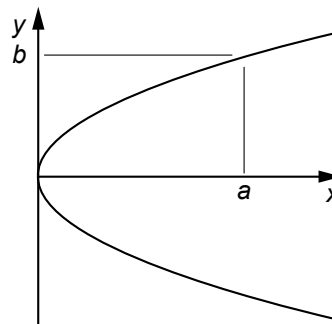
$$(x - a)^2 + (y - b)^2 = r^2$$



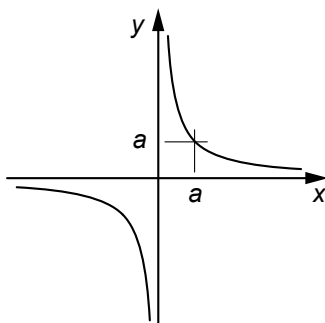
Ellipse:
 $\left(\frac{x}{a}\right)^2 + \left(\frac{y}{b}\right)^2 = 1$



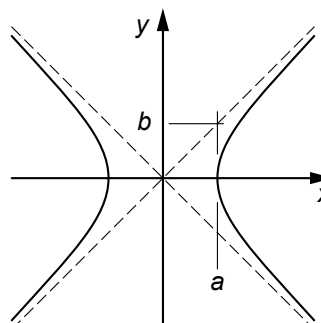
Parabola:
 $y = b \left(\frac{x}{a}\right)^2$



$$x = a \left(\frac{y}{b}\right)^2$$

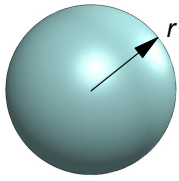


Hyperbola:
 $xy = a^2$

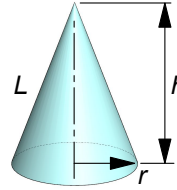


$$\left(\frac{x}{a}\right)^2 - \left(\frac{y}{b}\right)^2 = 1$$

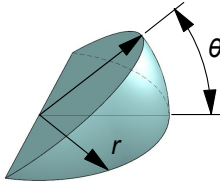
B.1.9 Solid geometry



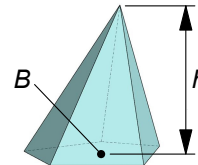
Sphere:
 volume = $\frac{4}{3}\pi r^3$
 surface area = $4\pi r^2$



Right-circular cone:
 volume = $\frac{1}{3}\pi r^2 h$
 lateral area = $\pi r L$
 $L = \sqrt{r^2 + h^2}$



Spherical wedge:
 volume = $\frac{2}{3}r^3\theta$



Any pyramid or cone:
 volume = $\frac{1}{3}Bh$
 where B = area of base.

B.1.10 Differential calculus

Leibnitz's rule:

$$D^n(fg) = f(D^n g) + n(Df)(D^{n-1}g) + \frac{n(n-1)}{2!}(D^2 f)(D^{n-2}g) + \dots + (D^n f)g$$

where $D = \frac{d}{dx}$, $f = f(x)$ and $g = g(x)$

Taylor's expansion of $f(x)$ about $x = a$:

$$f(x) = f(a) + (x-a)f'(a) + \frac{(x-a)^2}{2!}f''(a) + \dots + \frac{(x-a)^n}{n!}f^{(n)}(a) + \frac{(x-a)^{n+1}}{(n+1)!}f^{(n+1)}(\bar{x})$$

where $a < \bar{x} < x$. Substituting $h = x - a$ gives the following form:

$$f(a+h) = f(a) + hf'(a) + \frac{h^2}{2!}f''(a) + \dots + \frac{h^n}{n!}f^{(n)}(a) + R_n(h)$$

where $R_n(h) = \frac{h^{n+1}}{(n+1)!}f^{(n+1)}(a + \theta h)$, $(0 < \theta < 1)$.

Taylor's expansion of $f(x, y)$ about the point (a, b) :

$$\begin{aligned} f(x, y) = & f(a, b) + [(x-a)f_x + (y-b)f_y]_{a,b} \\ & + \frac{1}{2!} [(x-a)^2 f_{xx} + 2(x-a)(y-b)f_{xy} + (y-b)^2 f_{yy}]_{a,b} + \dots \end{aligned}$$

Substituting $h = x - a$ and $k = y - b$ gives the following form:

$$f(a+h, b+k) = f(a, b) + [hf_x + kf_y]_{a,b} + \frac{1}{2!} [h^2 f_{xx} + 2hkf_{xy} + k^2 f_{yy}]_{a,b} + \dots$$

Partial differentiation:

If $y = Y(x)$, then $f(x, y) = f[x, Y(x)] \equiv F(x)$ and

$$\frac{dF}{dx} = \frac{\partial f}{\partial x} + \frac{\partial f}{\partial y} \frac{dY}{dx}$$

If $x = X(t)$ and $y = Y(t)$, then $f(x, y) = F(t)$ and

$$\frac{dF}{dt} = \frac{\partial f}{\partial x} \frac{dX}{dt} + \frac{\partial f}{\partial y} \frac{dY}{dt}$$

If $x = X(u, v)$ and $y = Y(u, v)$ then $f(x, y) = F(u, v)$ and

$$\begin{aligned}\frac{\partial F}{\partial u} &= \frac{\partial f}{\partial x} \frac{\partial x}{\partial u} + \frac{\partial f}{\partial y} \frac{\partial y}{\partial u} \\ \frac{\partial F}{\partial v} &= \frac{\partial f}{\partial x} \frac{\partial x}{\partial v} + \frac{\partial f}{\partial y} \frac{\partial y}{\partial v}\end{aligned}$$

Stationary points of $f(x, y)$:

These occur where $f_x = 0$, $f_y = 0$ simultaneously. Let (a, b) be a stationary point: examine

$$K = \left[f_{xx}f_{yy} - (f_{xy})^2 \right]_{a,b}$$

If:

- $K < 0$, then (a, b) is a *saddle point*;
- $K > 0$ and $f_{xx}(a, b) < 0$, then (a, b) is a *maximum*;
- $K > 0$ and $f_{xx}(a, b) > 0$, then (a, b) is a *minimum*.

Radius of curvature in Cartesian coordinates:

$$\rho_{xy} = \frac{\left[1 + \left(\frac{dy}{dx} \right)^2 \right]^{3/2}}{\frac{d^2y}{dx^2}}$$

B.1.11 Standard Differentials

$f(x)$	$\frac{df(x)}{dx}$
x^n	nx^{n-1}
uv	$u \frac{dv}{dx} + v \frac{du}{dx}$
$\frac{u}{v}$	$\frac{v \frac{du}{dx} - u \frac{dv}{dx}}{v^2}$
$\sin x$	$\cos x$
$\cos x$	$-\sin x$
$\tan x$	$\sec^2 x$
$\sinh x$	$\cosh x$
$\cosh x$	$\sinh x$
$\tanh x$	$\text{sech}^2 x$
$\log_e x = \ln x$	$\frac{1}{x}$
e^{ax}	ae^{ax}

B.1.12 Differential equations

The first-order linear equation

$$\frac{dy}{dx} + R(x)y = S(x)$$

has an integrating factor

$$\lambda(x) = \exp \left[\int R(x) dx \right],$$

so that

$$\frac{d}{dx}(y\lambda) = S\lambda.$$

$$P(x, y) dx + Q(x, y) dy = 0$$

is an exact equation if

$$\frac{dP}{dy} = \frac{dQ}{dx}.$$

B.2 Integral calculus

An important substitution:

$$\tan \frac{\theta}{2} = t.$$

Then

$$\sin \theta = \frac{2t}{(1 + t^2)}$$

$$\cos \theta = \frac{(1 - t^2)}{(1 + t^2)}$$

and

$$d\theta = \frac{2}{(1 + t^2)} dt.$$

Table B.1: Some indefinite integrals

$f(x)$	$\int f(x) dx$
$\sec x$	$\ln(\sec x + \tan x) = \ln \tan \left(\frac{x}{2} + \frac{\pi}{4} \right)$
$\operatorname{cosec} x$	$\ln(\operatorname{cosec} x - \cot x) = \ln \tan \left(\frac{x}{2} \right)$
$(a^2 - x^2)^{-1/2}$	$\sin^{-1} \left(\frac{x}{a} \right), (x < a)$
$(a^2 + x^2)^{-1/2}$	$\sinh^{-1} \left(\frac{x}{a} \right) = \ln \left[x + (a^2 + x^2)^{1/2} \right] - \ln a = \ln \left[\frac{x}{a} + \left(1 + \left(\frac{x}{a} \right)^2 \right)^{1/2} \right]$
$(x^2 - a^2)^{-1/2}$	$\cosh^{-1} \left(\frac{x}{a} \right) = \ln \left[x + (x^2 - a^2)^{1/2} \right] - \ln a = \ln \left[\frac{x}{a} + \left(\left(\frac{x}{a} \right)^2 - 1 \right)^{1/2} \right], (x \geq a)$
$(a^2 + x^2)^{-1}$	$\frac{1}{a} \tan^{-1} \left(\frac{x}{a} \right)$
$(a^2 - x^2)^{-1}$	$\frac{1}{a} \tanh^{-1} \left(\frac{x}{a} \right) = \frac{1}{2a} \ln \left(\frac{a+x}{a-x} \right), (x < a)$
$(x^2 - a^2)^{-1}$	$\frac{1}{2a} \ln \left(\frac{x-a}{x+a} \right), (x > a)$

Table B.2: Some definite integrals

$I_n \equiv \int_0^{\pi/2} \sin^n x dx = \int_0^{\pi/2} \cos^n x dx = \frac{n-1}{n} I_{n-2}, \text{ where } I_0 = \frac{\pi}{2} \text{ and } I_1 = 1$
$I_{m,n} \equiv \int_0^{\pi/2} \sin^m x \cos^n x dx = \frac{m-1}{m+n} I_{m-2,n} = \frac{n-1}{m+n} I_{m,n-2}, (m > 1, n > 1)$
$\int_0^\infty e^{-ax} \sin bx dx = \frac{b}{(a^2 + b^2)}, (a > 0)$
$\int_0^\infty e^{-ax} \cos bx dx = \frac{a}{(a^2 + b^2)}, (a > 0)$
$\int_0^\infty e^{-x^2} dx = \frac{\sqrt{\pi}}{2}$

B.3 Laplace transforms

Function	Transform
Definition: $f(t)$	$\bar{f}(s) = \int_0^{\infty} e^{-st} f(t) dt$
$af(t) + bg(t)$	$a\bar{f}(s) + b\bar{g}(s)$
$\frac{df}{dt}$	$s\bar{f}(s) - f(0)$
$\frac{d^2f}{dt^2}$	$s^2\bar{f}(s) - sf(0) - f'(0)$
$e^{-at}f(t)$	$\bar{f}(s - a)$
$tf(t)$	$-\frac{d\bar{f}(s)}{ds}$
$\frac{\partial f(t, a)}{\partial a}$	$\frac{\partial \bar{f}(s, a)}{\partial a}$
$\int_0^t f(t) dt$	$\frac{\bar{f}(s)}{s}$
$\int_0^t f(u)g(t - u) du$	$\bar{f}(s)\bar{g}(s)$
$\delta(t_0)$, unit impulse at $t = t_0$	1
1, unit step	$\frac{1}{s} \quad (s > 0)$
$t^n, n = 1, 2, \dots$	$\frac{n!}{s^{n+1}} \quad (s > 0)$
e^{at}	$\frac{1}{s - a} \quad (s > a)$
e^{-at}	$\frac{1}{s + a}$
$\frac{1}{(n - 1)!} t^{n-1} e^{-at}$	$\frac{1}{(s + a)^n}$
$1 - e^{-at}$	$\frac{a}{s(s + a)}$
$\frac{1}{(b - a)} (e^{-at} - e^{-bt})$	$\frac{1}{(s + a)(s + b)}$
$\frac{1}{(b - a)} [(c - a)e^{-at} - (c - b)e^{-bt}]$	$\frac{s + c}{(s + a)(s + b)}$
$1 - \frac{b}{(b - a)} e^{-at} + \frac{a}{(b - a)} e^{-bt}$	$\frac{ab}{s(s + a)(s + b)}$
$\frac{e^{-at}}{(b - a)(c - a)} + \frac{e^{-bt}}{(c - a)(a - b)} + \frac{e^{-ct}}{(a - c)(b - c)}$	$\frac{1}{(s + a)(s + a)(s + b)}$
$c - \frac{b(c - a)}{(b - a)} e^{-at} + \frac{a(c - b)}{(b - a)} e^{-bt}$	$\frac{ab(s + c)}{s(s + a)(s + b)}$

Function	Transform
$\sin \omega t$	$\frac{\omega}{(s^2 + \omega^2)} \quad (s > 0)$
$\cos \omega t$	$\frac{s}{(s^2 + \omega^2)} \quad (s > 0)$
$\frac{\sqrt{(a^2 + \omega^2)}}{\omega} \sin(\omega t + \phi), \phi = \tan^{-1} \left(\frac{\omega}{a} \right)$	$\frac{s + a}{(s^2 + \omega^2)} \quad (s > 0)$
$e^{-at} \sin \omega t$	$\frac{\omega}{(s + a)^2 + \omega^2}$
$e^{-at} \cos \omega t$	$\frac{s + a}{(s + a)^2 + \omega^2}$
$\frac{1}{\omega} \sqrt{(c - a)^2 + \omega^2} e^{-at} \sin(\omega t + \phi), \phi = \tan^{-1} \left(\frac{\omega}{c - a} \right)$	$\frac{(s + c)}{(s + a)^2 + \omega^2}$
$\frac{\omega_n}{\sqrt{1 - \zeta^2}} e^{-\zeta \omega_n t} \sin \omega_n \sqrt{1 - \zeta^2} t, (\zeta < 1)$	$\frac{\omega_n^2}{s^2 + 2\zeta \omega_n s + \omega_n^2}$
$\frac{1}{a^2 + \omega^2} + \frac{1}{\omega \sqrt{a^2 + \omega^2}} e^{-at} \sin(\omega t - \phi), \phi = \tan^{-1} \frac{-\omega}{a}$	$\frac{1}{s[(s + a)^2 + \omega^2]}$
$1 - \frac{1}{\sqrt{1 - \zeta^2}} e^{-\zeta \omega_n t} \sin \left(\omega_n \sqrt{1 - \zeta^2} t + \phi \right), \phi = \cos^{-1} \zeta, \zeta < 1$	$\frac{\omega_n^2}{s(s^2 + 2\zeta \omega_n s + \omega_n^2)}$
$H(t - T) \quad (= 0, t < T; = 1, t > T)$	$\frac{1}{s} e^{-sT} \quad (s, T > 0)$

B.4 Numerical analysis

B.4.1 Approximate solution of an algebraic equation

- An iterative method for $x = \phi(x)$ converges when $|\phi'(x)| < 1$ near the root: if a root occurs near to $x = a$ take $x_0 = a$ and

$$x_{n+1} = \phi(x_n), n = 0, 1, 2, \dots$$

- If a root of $f(x) = 0$ occurs near to $x = a$, take $x_0 = a$ and:

$$x_{n+1} = x_n - \frac{f(x_n)}{f'(x_n)}, n = 0, 1, 2, \dots$$

(the *Newton-Raphson method*).

B.4.2 Numerical integration

Write $x_n = x_0 + nh$, $y_n = y(x_n)$. Then:

- Trapezium Rule (1 strip):

$$\int_{x_0}^{x_1} y(x) dx \approx \frac{h}{2} [y_0 + y_1]$$

- Simpson's Rule (2 strips):

$$\int_{x_0}^{x_1} y(x) dx \approx \frac{h}{3} [y_0 + 4y_1 + y_2]$$

B.4.3 Richardson's error estimation formula for use with Simpson's rule

Let

$$I = \int_a^b f(x) dx$$

and let I_1, I_2 be two estimates of I obtained using Simpson's rule with intervals h_1 and h_2 , where $h_1 < h_2$ (i.e. $h_1 = \frac{b-a}{n_1}$, $h_2 = \frac{b-a}{n_2}$, where n_1, n_2 are even). Then a better estimate of I is given by:

$$I = I_2 + \frac{(I_2 - I_1)}{\left[\left(\frac{h_1}{h_2}\right)^4 - 1\right]}.$$

If $h_2 = \frac{1}{2}h_1$ then $I = I_2 + \frac{1}{15}(I_2 - I_1)$.

B.4.4 Fourier series

If $f(x)$ is periodic of period $2L$, i.e. $f(x + 2L) = f(x)$, then

$$f(x) = \frac{a_0}{2} + \sum_{n=1}^{\infty} a_n \cos \frac{n\pi x}{L} + \sum_{n=1}^{\infty} b_n \sin \frac{n\pi x}{L}$$

where

$$a_n = \frac{1}{L} \int_{-L}^L f(x) \cos \frac{n\pi x}{L} dx, n = 0, 1, 2, \dots$$

$$b_n = \frac{1}{L} \int_{-L}^L f(x) \sin \frac{n\pi x}{L} dx, n = 1, 2, 3, \dots$$

If $f(x)$ is an *even* function of x , i.e. $f(-x) = f(x)$, then

$$a_n = \frac{2}{L} \int_0^L f(x) \cos \frac{n\pi x}{L} dx, b_n = 0, n = 0, 1, 2, \dots$$

If $f(x)$ is an *odd* function of x , i.e. $f(-x) = -f(x)$, then

$$b_n = \frac{2}{L} \int_0^L f(x) \sin \frac{n\pi x}{L} dx, a_n = 0, n = 1, 2, 3, \dots$$

B.5 Statistics

B.6 Probabilities for events

For events A , B and C :

$$P(A \cup B) = P(A) + P(B) - P(A \cap B)$$

The odds in favour of A are:

$$\frac{P(A)}{P(\bar{A})}$$

Conditional probability:

$$P(A|B) = \frac{P(A \cap B)}{P(B)} \quad (\text{if } P(B) > 0)$$

The chain rule:

$$P(A \cap B \cap C) = P(A)P(B|A)P(C|A \cap B)$$

Bayes' rule:

$$P(A|B) = \frac{P(A)P(B|A)}{P(A)P(B|A) + P(\bar{A})P(B|\bar{A})}$$

A and B are independent if

$$P(B|A) = P(B)$$

A , B and C are independent if

$$P(A \cap B \cap C) = P(A)P(B)P(C),$$

and $P(A \cap B) = P(A)P(B)$, $P(B \cap C) = P(B)P(C)$ and $P(C \cap A) = P(C)P(A)$.

B.6.1 Distribution, expectation and variance

The probability distribution for a discrete random variable X is the set $\{p_x\}$, where

$$p_x = P(X = x).$$

The expectation is

$$E(X) = \mu = \sum_x x p_x$$

From independent observations x_1, x_2, \dots, x_n , the sample mean

$$\bar{x} = \frac{1}{n} \sum_k x_k$$

estimates μ .

The variance is

$$\text{var}(X) = \sigma^2 = E\{(X - \mu)^2\} = E(X^2) - \mu^2,$$

where

$$E(X^2) = \sum_x x^2 p_x.$$

The *sample variance*:

$$s^2 = \frac{1}{n-1} \left\{ \sum_k x_k^2 - \frac{1}{n} \left(\sum_j x_j \right)^2 \right\}$$

estimates σ^2 .

The *standard deviation* is:

$$\text{sd}(X) = \sigma.$$

If the value y is observed with frequency n_y , then

$$n = \sum_y n_y, \quad \sum_k x_k = \sum_y y n_y, \quad \sum_k x_k^2 = \sum_y y^2 n_y.$$

For a function $g(x)$ of x ,

$$E \{g(x)\} = \sum_x g(x) p_x.$$

B.6.2 Probability distributions for a continuous random variable

The *cumulative distribution function* (cdf) is

$$F(x) = P(X \leq x) = \int_{x_0=-\infty}^x f(x_0) dx_0$$

The *probability density function* (pdf) is

$$f(x) = \frac{dF(x)}{dx}$$

$$\mu = \int_{-\infty}^{\infty} x f(x) dx, \quad \sigma^2 = E(X^2) - \mu^2$$

where

$$E(X^2) = \int_{-\infty}^{\infty} x^2 f(x) dx$$

B.6.3 Discrete probability distributions

Binomial distribution *Binomial* (n, θ)

$$p_x = \binom{n}{x} \theta^x (1 - \theta)^{n-x} \quad (x = 0, 1, 2, \dots, n)$$

$$\mu = n\theta, \quad \sigma^2 = n\theta(1 - \theta).$$

Poisson distribution *Poisson* (λ)

$$p_x = \frac{\lambda^x e^{-\lambda}}{x!} \quad (x = 0, 1, 2, \dots) \quad (\text{with } \lambda > 0)$$

$$\mu = \lambda, \quad \sigma^2 = \lambda.$$

B.6.4 Continuous probability distributions

Uniform distribution *Uniform* (α, β)

$$f(x) = \begin{cases} \frac{1}{\beta - \alpha} & (\alpha < x < \beta) \\ 0 & (\text{otherwise}). \end{cases} \quad \mu = \frac{\alpha + \beta}{2}, \sigma^2 = \frac{(\beta - \alpha)^2}{12}$$

Exponential distribution *Exponential* (λ)

$$f(x) = \begin{cases} \lambda e^{-\lambda x} & (0 < x < \infty), \\ 0 & (-\infty < x \leq 0). \end{cases} \quad \mu = \frac{1}{\lambda}, \sigma^2 = \frac{1}{\lambda^2}.$$

Normal distribution $N(\mu, \sigma^2)$

$$f(x) = \frac{1}{\sqrt{2\pi\sigma^2}} \exp \left\{ -\frac{1}{2} \left(\frac{x - \mu}{\sigma} \right)^2 \right\} \quad (-\infty < x < \infty), \quad E(X) = \mu, \quad \text{var}(X) = \sigma^2$$

Standard normal distribution is $N(0, 1)$

If X is $N(\mu, \sigma^2)$, then $Y = \frac{X - \mu}{\sigma}$ is $N(0, 1)$.

B.6.5 System reliability

For a system of k devices, which operate independently, let

$$R_i = P(D_i) = P(\text{"device } i \text{ operates"}).$$

The *system reliability*, R , is the probability of a path of operating devices.

A system of devices *in series* fails if any device fails:

$$R = P(D_1 \cap D_2 \cap \dots \cap D_k) = R_1 R_2 \dots R_k$$

A system of devices *in parallel* operates if any device operates:

$$R = P(D_1 \cup D_2 \cup \dots \cup D_k) = 1 - (1 - R_1)(1 - R_2) \dots (1 - R_k)$$

B.7 Bias, standard error and mean square error

If t estimates θ and comes from a distribution having random variable T :

- *Bias* of t : $\text{bias}(t) = E(T) - \theta$
- *Standard error* of t : $\text{se}(t) = \text{sd}(t)$
- *Mean square error* of t : $\text{MSE}(t) = E\{(t - \theta)^2\} = \{\text{se}(t)\}^2 + \{\text{bias}(t)\}^2$

if \bar{x} estimates μ , then $\text{bias}(\bar{x}) = 0$, $\text{se}(\bar{x}) = \frac{\sigma}{\sqrt{n}}$, $\text{MSE}(\bar{x}) = \frac{\sigma^2}{n}$, $\widehat{\text{se}}(\bar{x}) = \frac{s}{\sqrt{n}}$

B.7.1 Central limit property

If n is fairly large, \bar{x} is approximately from $N\left(\mu, \frac{\sigma^2}{n}\right)$.

B.7.2 Confidence intervals

If x_1, x_2, \dots, x_n are independent observations from $N(\mu, \sigma^2)$ and σ^2 is known, then the 95% confidence interval for μ is $\left(\bar{x} - 1.96 \frac{\sigma}{\sqrt{n}}, \bar{x} + 1.96 \frac{\sigma}{\sqrt{n}}\right)$.

If σ^2 is estimated then, from the table of $t_{(n-1)}$, we find $t_0 = t_{(n-1), 0.05}$. Then the 95% CI for μ is $\left(\bar{x} - t_0 \frac{s}{\sqrt{n}}, \bar{x} + t_0 \frac{s}{\sqrt{n}}\right)$.

y	$\phi(y)$	$\Phi(y)$	y	$\phi(y)$	$\Phi(y)$	y	$\phi(y)$	$\Phi(y)$	y	$\Phi(y)$
0	0.399	0.5	0.9	0.266	0.816	1.8	0.079	0.964	2.8	0.997
0.1	0.397	0.540	1.0	0.242	0.841	1.9	0.066	0.971	3.0	0.998
0.2	0.391	0.579	1.1	0.218	0.864	2.0	0.054	0.977	0.841	0.8
0.3	0.381	0.618	1.2	0.194	0.885	2.1	0.044	0.982	1.282	0.9
0.4	0.368	0.655	1.3	0.171	0.903	2.2	0.035	0.986	1.645	0.95
0.5	0.352	0.691	1.4	0.150	0.919	2.3	0.028	0.989	1.96	0.975
0.6	0.333	0.726	1.5	0.130	0.933	2.4	0.022	0.992	2.326	0.99
0.7	0.312	0.758	1.6	0.111	0.945	2.5	0.018	0.994	2.576	0.995
0.8	0.290	0.788	1.7	0.094	0.955	2.6	0.014	0.995	3.09	0.999

Table B.3: Standard normal table: values of pdf $\phi(y) = f(y)$ and cdf $\Phi(y) = F(y)$.

p	0.10	0.05	0.02	0.01		p	0.10	0.05	0.02	0.01	
m	1	6.31	12.71	31.82	63.66	m	9	1.83	2.26	2.82	3.25
	2	2.92	4.30	6.96	9.92		10	1.81	2.23	2.76	3.17
	3	2.35	3.18	4.54	5.84		12	1.78	2.18	2.68	3.05
	4	2.13	2.78	3.75	4.60		15	1.75	2.13	2.60	2.95
	5	2.02	2.57	3.36	4.03		20	1.72	2.09	2.53	2.85
	6	1.94	2.45	3.14	3.71		25	1.71	2.06	2.48	2.78
	7	1.89	2.36	3.00	3.50		40	1.68	2.02	2.42	2.70
	8	1.86	2.31	2.90	3.36		∞	1.645	1.96	2.326	2.576

Table B.4: Student t table: values $t_{m,p}$ of x for which $P(|X| > x) = p$, when X is t_m .

C Mechatronics and control

Data and formulae for core course examinations in:

- Mechatronics
- Dynamics
- Machine System Dynamics

and in other, related, optional courses.

C.1 Charge, current, voltage and power

q = charge

i = current = $\frac{dq}{dt}$

v = electrical potential (*voltage*)

P = power leaving network

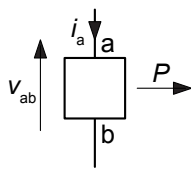
U = energy stored

R = resistance

C = capacitance

L = inductance

Subscript and arrow notations



Potential difference:

$$v_{ab} = v_a - v_b$$

Power P leaving network between terminals a and b:

$$P = v_{ab} i_a$$

Passive components

Resistor: $v = iR$ (Ohm's law) Power dissipated: $P = i^2 R = \frac{v^2}{R}$

Inductor: $v = L \frac{di}{dt}$ Energy stored $U = \frac{1}{2} L i^2$

Capacitor: $i = C \frac{dv}{dt}$, $q = Cv$ Energy stored $U = \frac{1}{2} C v^2$

Table C.1: Colour codes for resistors etc.

Colour	Digit		
Black	0	Green	5
Brown	1	Blue	6
Red	2	Violet	7
Orange	3	Grey	8
Yellow	4	White	9

Table C.2: Standard values for components

E3 series	E6 series	E12 series	E24 series
10	10	10	10
			11
		12	12
			13
	15	15	15
			16
		18	18
			20
22	22	22	22
			24
		27	27
			30
	33	33	33
			36
		39	39
			43
47	47	47	47
			51
		56	56
			63
	68	68	68
			75
		82	82
			91

C.2 Networks

Kirchhoff's voltage law (KVL):

$$\sum (\text{p.d.s around loop}) = 0$$

Kirchhoff's current law (KCL):

$$\sum (\text{currents into node}) = 0$$

Resistors in series:

$$R_{\text{ser}} = R_1 + R_2 + \dots$$

Resistors in parallel:

$$\frac{1}{R_{\text{par}}} = \frac{1}{R_1} + \frac{1}{R_2} + \dots$$

i.e. for two resistors

$$R_{\text{par}} = \frac{R_1 R_2}{R_1 + R_2}$$

Potential divider (with R_2 as output resistor):

$$V_{\text{out}} = \frac{R_2}{R_1 + R_2} V_{\text{in}}$$

C.3 Transients

- $x(t)$ = instantaneous voltage v or current i
- X_0 = initial value $x(0)$
- X_f = final (steady state) value $x(\infty)$.
- τ = time constant.

At time $t = 0$ a switch operates so that the network of resistors and d.c. voltage sources connected to a capacitor or inductor changes, instantaneously. Then for $t \geq 0$:

$$x(t) = X_f - (X_f - X_0) \exp\left(-\frac{t}{\tau}\right)$$

For a capacitor:

- v remains unchanged through $t = 0$;
- $i \rightarrow 0$ as $t \rightarrow \infty$;
- $\tau = R_s C$

For an inductor:

- i remains unchanged through $t = 0$;
- $v \rightarrow 0$ as $t \rightarrow \infty$;
- $\tau = \frac{L}{R}$

C.4 AC networks

- X_m = *peak amplitude* (or semi-amplitude)
- X_{av} = mean value $x(\infty)$.
- X_{pp} = $2X_m$ is *peak-to-peak* amplitude
- f = frequency (Hz), and $\omega = 2\pi f$ (rad s^{-1})
- T = $\frac{1}{f}$ is period

C.4.1 Average and root mean square values

General definitions for any periodic waveform:

$$X_{\text{av}} = \frac{1}{T} \int_0^T x \, dt$$

$$X_{\text{rms}} = \sqrt{\frac{1}{T} \int_0^T x^2 \, dt}$$

For a waveform consisting of N samples of equal duration:

$$X_{\text{rms}} = \sqrt{\frac{1}{N} \sum_{n=1}^N x_n^2 dt}$$

For a sinusoidal waveform $x = X_m \sin(\omega t + \phi)$:

$$X_{\text{rms}} = \frac{1}{\sqrt{2}} X_m$$

and for a sinusoidal positive half-cycle:

$$X_{\text{av}} = \frac{2}{\pi} X_m$$

C.4.2 Phasors and complex impedance

CIVIL: current leads voltage for a capacitor, voltage leads current for an inductor.

Current is common phasor for series circuits, voltage is common phasor for parallel circuits.

Inductive reactance: $X_L = \omega L$;

Capacitive reactance $X_C = \frac{1}{\omega C}$.

Complex impedance: $\bar{V} = \bar{I} \cdot \bar{Z}$ where \bar{V} , \bar{I} , and \bar{Z} are complex quantities, and

$$\bar{Z} = R \pm jX$$

where \bar{X} is impedance.

C.4.3 Balanced 3 phase a.c supply

Relationships between line voltage V_L and current I_L , phase voltage V_P and current I_P for star connected load

$$V_L = \sqrt{3}V_P, \quad I_L = I_P$$

and for delta connected load:

$$V_L = V_P, \quad I_L = \sqrt{3}I_P$$

C.4.4 Electromagnetism

- N = number of coil turns
- H = magnetic field strength
- l = magnetic flux path length
- ϕ = magnetic flux
- B = magnetic flux density
- μ_r = relative permeability
- μ_0 = permittivity of free space
- A = cross-sectional area of magnetic flux path.
- L = length of conductor in magnetic field.
- U = velocity of conductor

Magnetomotive force (m.m.f.) = iN , $H = \frac{\text{m.m.f.}}{l}$

$$B = \frac{\Phi}{A} = \mu_r \mu_0 H (\text{tesla})$$

Reluctance of magnetic path:

$$S = \frac{\text{m.m.f.}}{\Phi} = \frac{l}{\mu_r \mu_0 A}$$

Magnetic force of attraction:

$$F = \frac{B^2 A}{2\mu_0}$$

Force acting on a conductor:

$$F = BiL$$

Induced e.m.f.:

$$E = BLU = \frac{d\Phi}{dt}$$

C.4.5 DC machines

- T_0 = shaft torque
- K_e = e.m.f. constant
- R_a = armature resistance
- v_a = armature voltage
- i_a = armature current
- ω = angular velocity

Torque-speed relationship for a permanent-magnet or shunt-wound d.c. machine:

$$\omega = \frac{1}{K_e} v_a - \frac{R_a}{K_e^2} T_0$$

and $T_0 = K_e i_a$.

C.4.6 Transformers

- Φ = peak flux
- f = frequency
- N_1, N_2 = primary and secondary turns

Ideal transformer:

$$\frac{V_1}{V_2} = \frac{N_1}{N_2} = \frac{I_2}{I_1}$$

RMS value of induced e.m.f.:

$$E = 4.44 N f \Phi$$

C.5 Communications

Information (in bits) communicated by each of N equally probable messages:

$$I = \frac{1}{\log_{10} 2} \log N$$

Information (in bits) communicated by a message of probability P :

$$I = \frac{1}{\log_{10} 2} \log \left(\frac{1}{P} \right)$$

C.6 Step function response and frequency response

$\theta_{in}, \theta_{out}$ = input and output variables

τ = time constant

ω_n = natural frequency

ζ = damping factor

H = gain

ϕ = phase shift

The *transfer function* for any linear system is generally expressed as a linear function of the Laplace variable s .

C.6.1 First-order systems

Transfer function of first order low pass (lag):

$$\frac{\theta_{out}}{\theta_{in}} = \frac{1}{1 + \tau s}$$

Figure C.1 shows the time plot for response to a unit step input:

$$\theta_{in} = \begin{cases} 0 & (t < 0) \\ 1 & (t > 0) \end{cases}$$

Gain (power ratio) in decibels (dB): $|H| = 20 \log_{10} \left(\frac{V_{out}}{V_{in}} \right)$.

Figure C.2 shows the Bode plots for sinusoidal input $\theta_{in} = \hat{\theta}_{in} \sin(\omega t - \phi)$ to first-order low-pass and high-pass filters. For *active* filters (see Table C.3):

	Low-pass filter	High-pass filter
Passive	$ H = \frac{1}{\sqrt{1 + (\omega RC)^2}}$ $\phi = -\tan^{-1}(\omega RC)$	$ H = \frac{\omega RC}{\sqrt{1 + (\omega RC)^2}}$ $\phi = 90^\circ - \tan^{-1}(\omega RC)$
Active	$ H = \frac{R_2}{R_1} \frac{1}{\sqrt{1 + (\omega R_2 C)^2}}$ $\phi = 180^\circ - \tan^{-1}(\omega R_2 C)$	$ H = \frac{C_1}{C_2} \frac{\omega RC_2}{\sqrt{1 + (\omega RC_2)^2}}$ $\phi = -90^\circ - \tan^{-1}(\omega RC)$

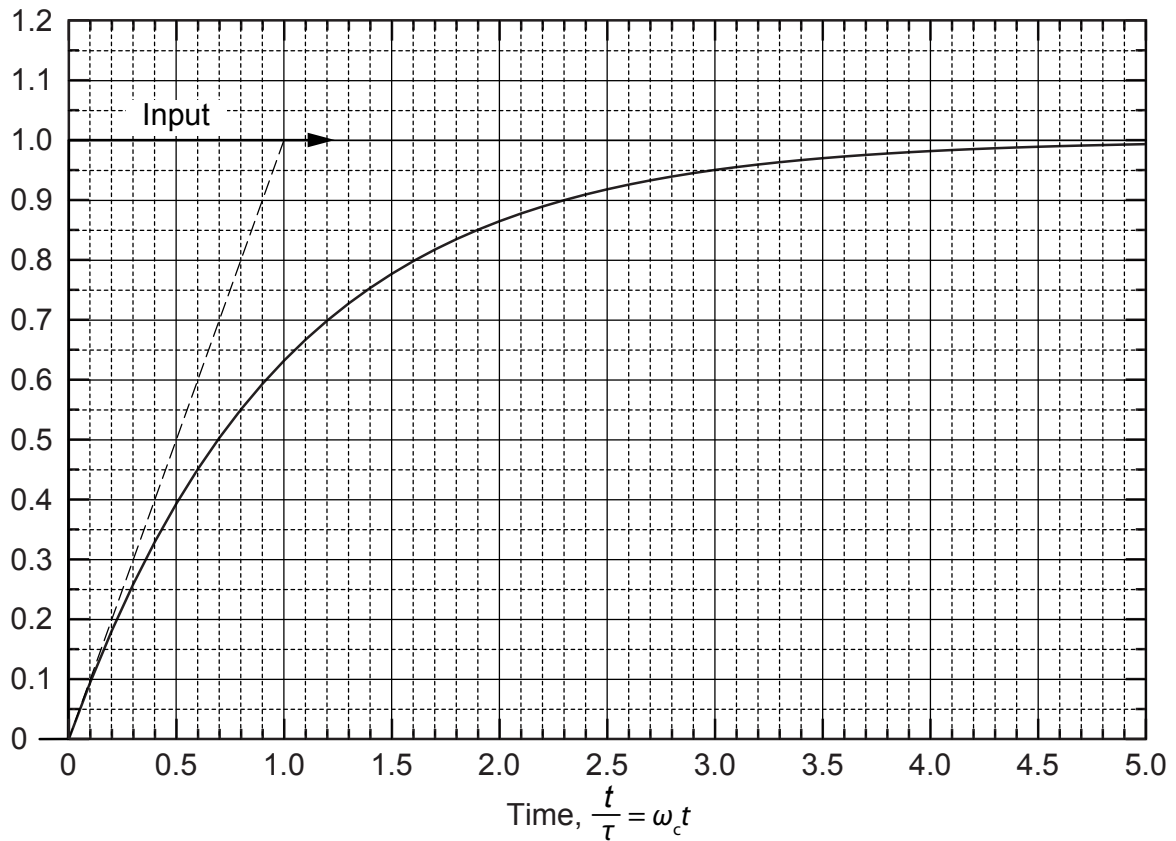


Figure C.1: Step response of a first-order low pass filter

C.6.2 Second-order systems

Transfer function of a second-order low-pass system:

$$\frac{\theta_{\text{out}}}{\theta_{\text{in}}} = \frac{1}{\left(1 + 2\frac{\zeta}{\omega_n}s + \frac{1}{\omega_n^2}s^2\right)}$$

Unit step and frequency response are shown in Figs. C.3 and C.4.

C.7 Operational amplifier stages

Table C.3 shows op-amp networks which implement various signal processing operations.

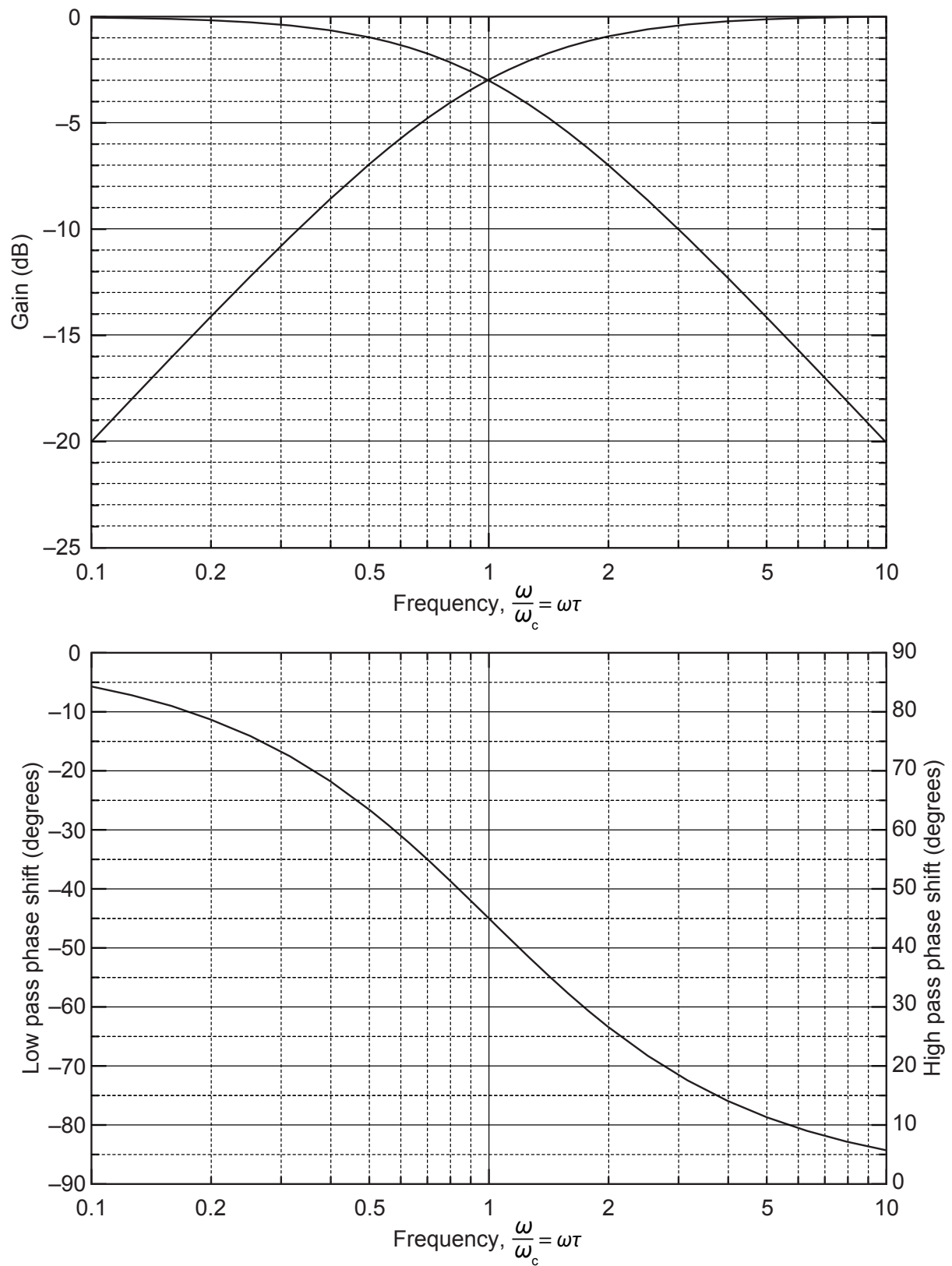


Figure C.2: Bode plot for first-order low and high pass filters

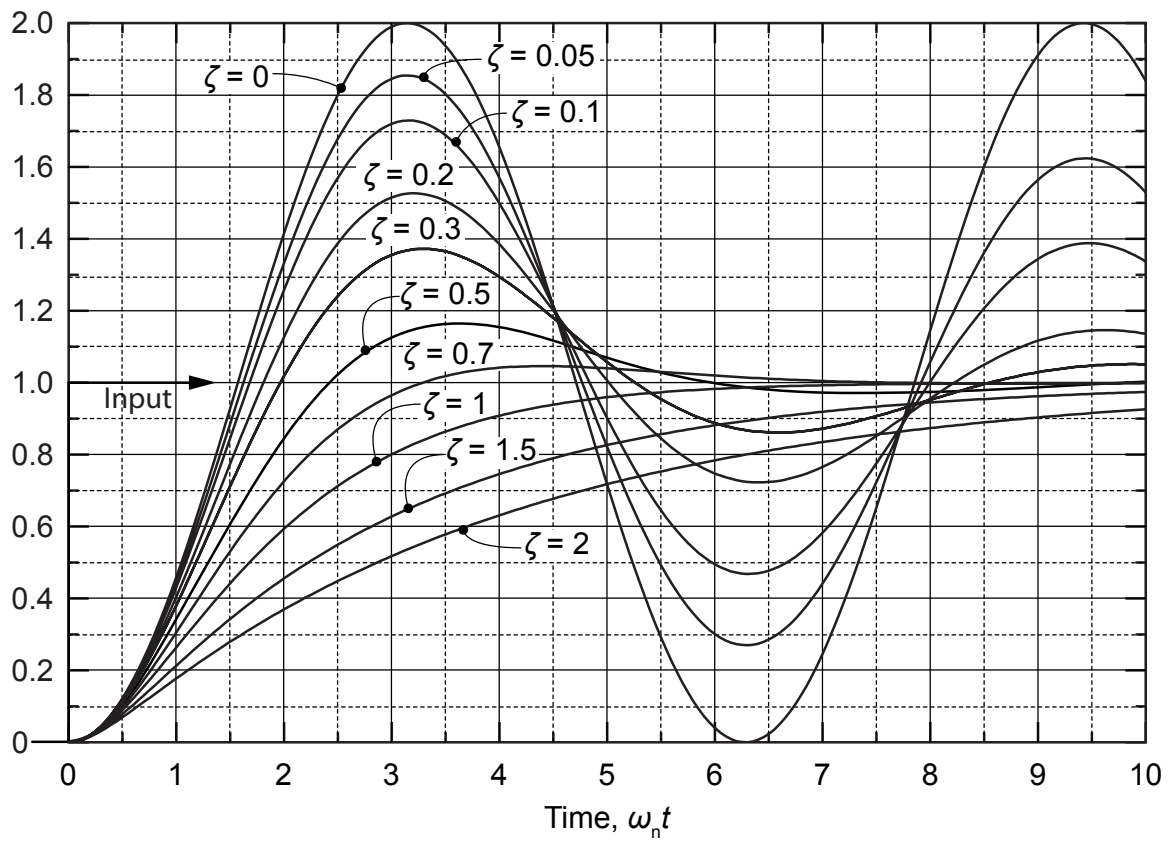


Figure C.3: Step response of a second-order low pass filter

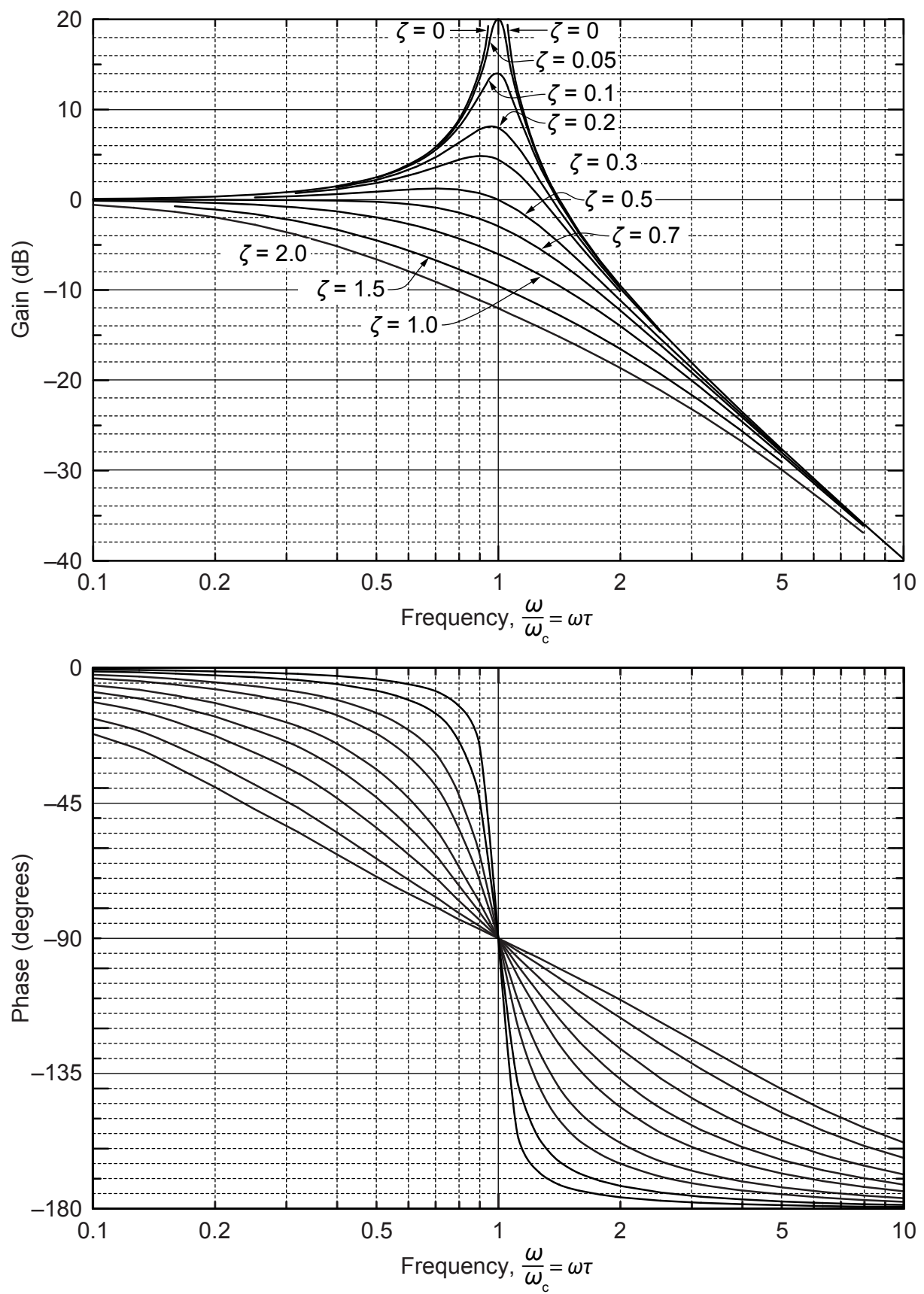
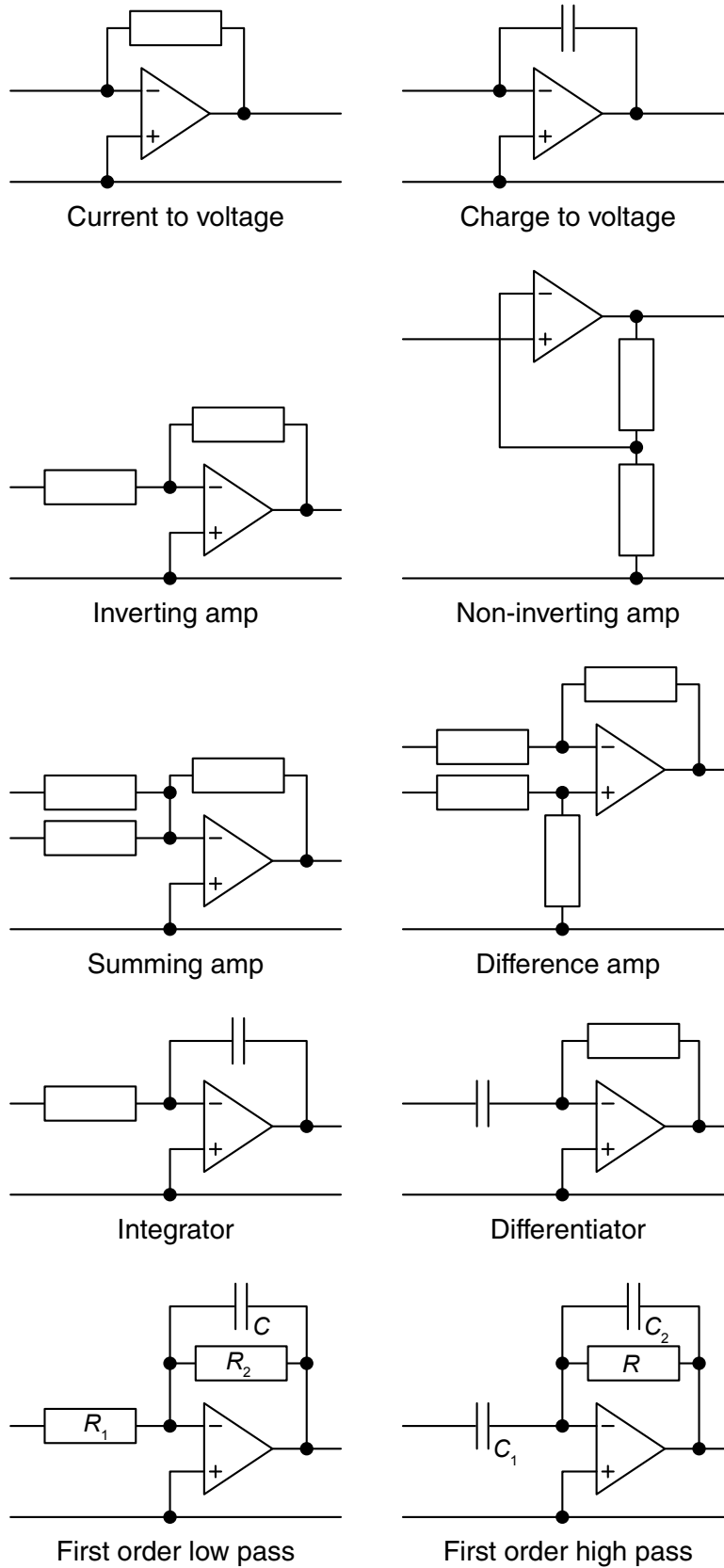


Figure C.4: Bode plot for a second-order low pass filter

Table C.3: Operational amplifier signal processing stages



D Solid Mechanics

Data and formulae for core course examinations in:

- Mechanics
- Stress Analysis
- Materials

and in other, related, optional courses.

D.1 Mechanics

D.1.1 Square screw threads

- M = moment required to *raise* an axially loaded nut
 W = axial load on nut
 ϕ = helix angle of thread
 μ_s = static coefficient of friction
 d_m = mean thread diameter

$$M = \left(\frac{\tan \phi + \mu_s}{1 - \mu_s \tan \phi} \right) W \frac{d_m}{2}$$

D.1.2 Flat clutches

- T = maximum torque transmitted
 F = thrust
 R_1, R_2 = outer and inner radii for annular clutch
 μ_s = static coefficient of friction

For uniform pressure conditions:

$$T = \frac{2}{3} \mu_s F \left(\frac{R_1^3 - R_2^3}{R_1^2 - R_2^2} \right)$$

For uniform wear conditions:

$$T = \mu_s F \left(\frac{R_1 + R_2}{2} \right)$$

D.1.3 Kinematics of particle

- \mathbf{a} = acceleration vector
 s = distance travelled
 v = tangential velocity
 t = time
 $\mathbf{e}_n, \mathbf{e}_t$ = unit vectors in n - t coordinates
 $\mathbf{e}_r, \mathbf{e}_\theta$ = unit vectors in r - θ coordinates
 ρ = instantaneous radius of path curvature

For normal and tangential components:

$$\mathbf{a} = \frac{d^2s}{dt^2} \mathbf{e}_t + \frac{v^2}{\rho} \mathbf{e}_n$$

For polar components:

$$\mathbf{a} = (\ddot{r} - r\dot{\theta}^2) \mathbf{e}_r + (r\ddot{\theta} + 2\dot{r}\dot{\theta}) \mathbf{e}_\theta$$

D.1.4 Mass flow problems

- \mathbf{F} = internal force vector exerted from the emitted mass
- \mathbf{a} = acceleration vector
- m = mass of object
- m_f = emitted mass
- \mathbf{v}_f = velocity vector of emitted mass relative to object

$$m\mathbf{a} = -\frac{dm_f}{dt} \mathbf{v}_f = \mathbf{F}$$

D.1.5 Kinematics of rigid bodies with sliding contacts

- \mathbf{v} = velocity vector
- \mathbf{a} = acceleration vector
- \mathbf{v}_{rel} = velocity vector relative to rotating body (sliding velocity)
- \mathbf{a}_{rel} = acceleration vector relative to rotating body (sliding acceleration)
- $\boldsymbol{\omega}$ = angular velocity vector
- $\boldsymbol{\alpha}$ = angular acceleration vector
- \mathbf{r} = position vector

$$\mathbf{v} = \mathbf{v}_{\text{rel}} + \boldsymbol{\omega} \times \mathbf{r}$$

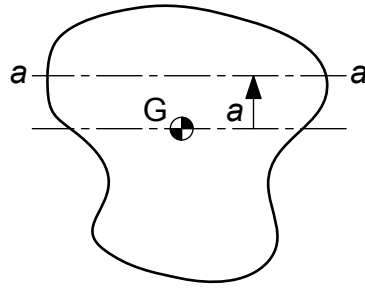
$$\mathbf{a} = \mathbf{a}_{\text{rel}} + 2\boldsymbol{\omega} \times \mathbf{v}_{\text{rel}} + \boldsymbol{\alpha} \times \mathbf{r} + \boldsymbol{\omega} \times (\boldsymbol{\omega} \times \mathbf{r})$$

D.1.6 Mass moments of inertia

- M = total mass of body
- G = centre of mass (centre of gravity)
- I_G = Mass moment of inertia about G
- I_{aa} = Mass moment of inertia about an axis $a - a$

	Body	Mass moment of inertia
	Rectangular lamina, $b \times h$	$I_G = \frac{1}{12}M(b^2 + h^2)$
	Circular lamina, radius r	$I_G = \frac{1}{2}Mr^2$
	Uniform slender rod, total length L	$I_G = \frac{1}{12}ML^2$
	Sphere, radius r	$I_G = \frac{2}{5}Mr^2$

Parallel axis theorem:



$$I_{aa} = I_G + Ma^2$$

D.2 Stress analysis

D.2.1 Elastic constants of materials

- ρ = Density
- E = Young's modulus, modulus of elasticity
- G = Shear modulus, modulus of rigidity
- K = Bulk modulus
- ν = Poisson's ratio
- α = Coefficient of linear thermal expansion

Relationships between elastic constants:

$$G = \frac{E}{2(1 + \nu)} \quad K = \frac{E}{3(1 - 2\nu)}$$

Some typical values:

	ρ kg m^{-3}	E GPa	G GPa	K GPa	ν	α $\times 10^6 \text{ K}^{-1}$
Mild steel	7850	207	79.6	175	0.3	11
Aluminium alloy	2720	68.9	26.5	69	0.3	23
Brass	8410	103	38.3	117	0.35	19
Titanium alloy	5000	110	42		0.31	11
Softwood along grain		9				
Water	1000			2.2		
Concrete	2400	13.8			0.1	

D.2.2 Beam theory

- σ = axial stress at axial position z and vertical distance y from neutral axis
- τ = shear stress in vertical \times axial plane
- d = total depth of beam
- M = bending moment about neutral axis at z
- S = shear force at z
- I = second moment of area about neutral axis
- R = radius of curvature at z
- v = vertical deflection at z

Bending about a principal axis :

$$\frac{\sigma}{y} = \frac{M}{I} = \frac{E}{R} = E \frac{d^2 v}{dz^2}$$

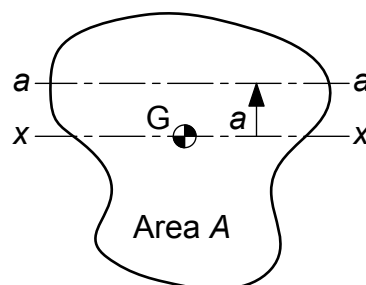
and

$$\tau = \frac{S}{2I} \left(\frac{d^2}{4} - y^2 \right)$$

Table D.1: Second moments of area for simple cross-sections

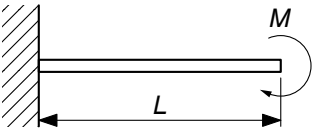
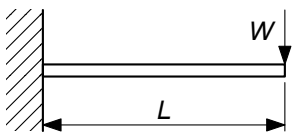
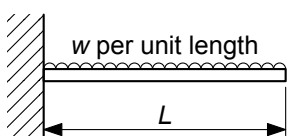
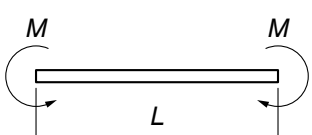
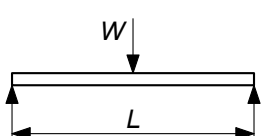
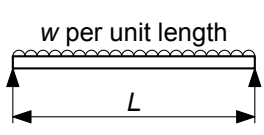
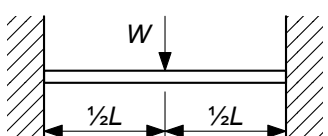
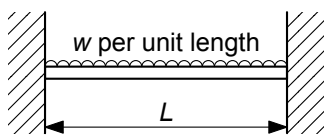
	$I_{xx} = \frac{1}{12} b d^3$ $I_{yy} = \frac{1}{12} b^3 d$
	$I_{xx} = I_{yy} = \frac{1}{4} \pi a^4$
	$I_{xx} = \frac{1}{36} (b_1 + b_2) h^3$ $I_{yy} = \frac{1}{36} (b_1 + b_2) (b_1^2 + b_1 b_2 + b_2^2)$

Parallel axis theorem:



$$I_{aa} = I_{xx} + Aa^2$$

Table D.2: Beams bent about principal axis

	End slope	End deflection	Central deflection
	$\frac{ML}{EI}$	$\frac{ML^2}{2EI}$	
	$\frac{WL^2}{2EI}$	$\frac{WL^3}{3EI}$	
	$\frac{wL^3}{6EI}$	$\frac{wL^4}{8EI}$	
	$\frac{ML}{2EI}$		$\frac{ML^2}{8EI}$
	$\frac{WL^2}{16EI}$		$\frac{WL^3}{48EI}$
	$\frac{wL^3}{24EI}$		$\frac{5wL^4}{384EI}$
	End moment	Central deflection	
	$\frac{WL}{8}$	$\frac{WL^3}{192EI}$	
	$\frac{WL^2}{12}$	$\frac{WL^4}{384EI}$	

D.2.3 Elastic torsion

Circular solid and hollow shafts

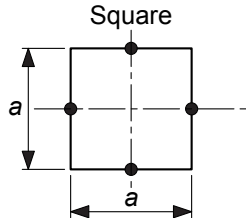
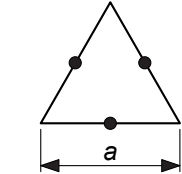
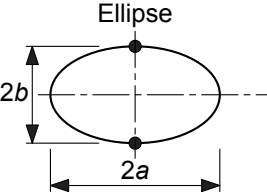
- τ = shear stress at radius r
 T = applied torque
 J = polar second moment of area
 d = diameter of circular section
 θ = angle of twist over length L

$$\frac{\tau}{r} = \frac{T}{J} = \frac{G\theta}{L}$$

For a solid circular section:

$$J = 2I_{xx} = \frac{\pi d^4}{32}$$

Table D.3: Torsion of solid non-circular sections

Shape of cross section	Maximum shear stress, τ_{\max}	Angle of twist, θ
<p>Square</p> 	$4.81 \frac{T}{a^3}$	$7.10 \frac{TL}{a^4 G}$
<p>Equilateral triangle</p> 	$20 \frac{T}{a^3}$	$46 \frac{TL}{a^4 G}$
<p>Ellipse</p> 	$\frac{2}{\pi} \frac{T}{ab^2}$	$(a^2 + b^2) \frac{TL}{\pi a^3 b^3 G}$

Thin walled tubes of arbitrary cross-section

- A = enclosed area to mid-thickness
 t = wall thickness
 s = distance around perimeter

$$\tau = \frac{T}{2At}$$

Torsional stiffness:

$$\frac{T}{\theta/l} = \frac{4A^2G}{\oint \left(\frac{1}{t}\right) ds}$$

Springs

- d = wire diameter
 D = helix diameter
 δ = deflection
 F = force

End deflection of a closed-helix, round wire spring:

$$\delta = \frac{8FD^3N}{Gd^4}$$

Maximum shear stress (torsion only):

$$\tau = \frac{8FD}{\pi d^3}$$

D.2.4 Thin walled pressure vessels

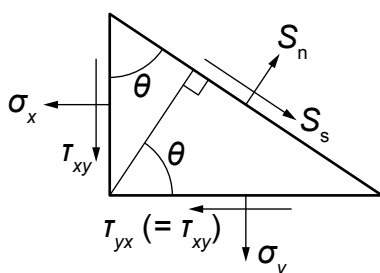
- R = mean radius
 t = wall thickness
 p = internal pressure

Hoop stress in hollow, pressurised cylinder:

$$\sigma_\theta = p \left(\frac{R}{t} \right)$$

Stress in hollow, pressurised sphere :

$$\sigma = p \left(\frac{R}{2t} \right)$$

D.3 Two-dimensional stress transformation

$$S_n = \frac{\sigma_x + \sigma_y}{2} + \frac{\sigma_x - \sigma_y}{2} \cos 2\theta + \tau_{xy} \sin 2\theta$$

$$S_s = \frac{\sigma_x - \sigma_y}{2} \sin 2\theta - \tau_{xy} \cos 2\theta$$

Principal stresses:

$$\sigma_1, \sigma_2 = \frac{\sigma_x + \sigma_y}{2} \pm \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$$

The direction of the principal stresses (and of the normal to the principal planes) to the x axis is θ_p where:

$$\tan 2\theta_p = \frac{2\tau_{xy}}{\sigma_x - \sigma_y}$$

Maximum shear stress: The maximum shear stress is half the difference of the principal stresses and acts on planes at 45° to the principal planes.

D.4 Yield criteria

- Y = yield stress in uniaxial tension
- t = wall thickness

In a three dimensional stress system having principal stresses σ_1 , σ_2 and σ_3 where

$$\sigma_1 \geq \sigma_2 \geq \sigma_3.$$

Tresca yield criterion:

$$|\sigma_1 - \sigma_3| = Y$$

Von Mises yield criterion:

$$(\sigma_1 - \sigma_2)^2 + (\sigma_2 - \sigma_3)^2 + (\sigma_3 - \sigma_1)^2 = 2Y^2$$

D.5 Two-dimensional strain transformation

$$e_n = \frac{e_x + e_y}{2} + \frac{e_x - e_y}{2} \cos 2\theta + \frac{\gamma_{xy}}{2} \sin 2\theta$$

$$\frac{e_s}{2} = \frac{e_x - e_y}{2} \sin 2\theta - \frac{\gamma_{xy}}{2} \cos 2\theta$$

where:

- e_x , e_y and e_n are the direct strains acting in the same directions as, respectively, the stresses s_x , s_y and S_n above;
- γ_{xy} and e_s are the shear strains associated with the stresses τ_{xy} and S_s

NOTE: the relevant strain relationships may be obtained from the stress relationships by substituting the appropriate direct stresses by the associated direct strain and shear stresses by *one half* of the associated shear strain.

D.6 Elastic stress-strain relationships

$$e_x = \frac{1}{E} (\sigma_x - \nu (\sigma_y + \sigma_z)) \text{ etc}$$

$$\gamma_{xy} = \frac{1}{G} \tau_{xy} \text{ etc}$$

D.7 Thick-walled cylinders

For axi-symmetric systems, the circumferential and radial stresses at radius r are, respectively:

$$\sigma_{\theta\theta} = A + \frac{B}{r^2}$$

$$\sigma_{rr} = A - \frac{B}{r^2}$$

E Thermofluids

Data and formulae for core course examinations in:

- Fluid Mechanics
- Thermodynamics
- Heat Transfer
- Thermodynamics and Energy

and in other, related, optional courses.

E.1 Cross-references to table numbers

Some Tables in this handbook are referred to by different numbers in lecture notes and problem sheets.

External reference	Table number in this handbook
Table E1	Table E.1
Table E2	Table E.2
Table E3	Section E.4
Table E4	Section E.5
Table E5	Table E.3
Table E6	Table E.4
Table E7a	Table E.5
Table E7b	Table E.6
Table E7c	Table E.7
Table E8	Tables E.8 and E.9
Table E9a	Table E.16
Table E9b	Table E.17
Table E10	Table E.18
Table R1	Table E.10
Table R2	Table E.11
Table R3 Part 1	Table E.12
Table R3 Part 2	Table E.13
Table R3 Part 3	Table E.14
Table R3 Part 4	Table E.15
Table S1	Table E.19
Table S2	Tables E.20 to E.22
Table S3	Tables E.23 to E.29

E.2 Dimensionless groups

A	=	surface area
C_p	=	specific heat at constant pressure
D	=	pipe diameter
F_D, F_L	=	drag force, lift force
g	=	gravitational acceleration
h	=	surface heat-transfer coefficient
k_f, k_s	=	thermal conductivity of fluid, of solid
L	=	reference length
ΔP	=	pressure drop
T_∞, T_s	=	temperature at infinity, at surface
U	=	characteristic velocity
α	=	thermal diffusivity
β	=	coefficient of volumetric thermal expansion
ε	=	roughness height
μ	=	absolute viscosity
ρ	=	density

Table E.1: Dimensionless groups for Thermofluids

Parameter	Definition
Biot number (Bi)	$\frac{hL}{k_s}$
Coefficient of lift (C_L)	$\frac{F_L}{\frac{1}{2}\rho U^2 A}$
Coefficient of drag (C_D)	$\frac{F_D}{\frac{1}{2}\rho U^2 A}$
Fourier number (Fo)	$\frac{\alpha t}{L^2}$
Friction factor (f)	$\frac{\Delta P}{\left(\frac{L}{D}\right)^{\frac{1}{2}}\rho U^2}$
Grashof number (Gr)	$\frac{\beta g (T_\infty - T_s) L^3 \rho^2}{\mu^2}$
Nusselt number (Nu)	$\frac{hL}{k_f}$
Prandtl number (Pr)	$\frac{\mu C_p}{k_f}$
Rayleigh number (Ra)	$\text{Gr} \cdot \text{Pr}$
Reynolds number (Re)	$\frac{UL\rho}{\mu}$
Roughness ratio	$\frac{\varepsilon}{L}$
Stanton number (St)	$\frac{h}{\rho U C_p} = \frac{\text{Nu}}{\text{Re} \cdot \text{Pr}}$

E.3 Heat transfer

Table E.2: Empirical correlations for forced convection

Correlation	Conditions
Laminar flow over a flat plate:	
$C_f(x) = \frac{0.664}{\text{Re}_x^{1/2}}$	$\text{Pr} \geq 0.6$
$\text{Nu}(x) = \frac{h(x)x}{k} = 0.332\text{Re}_x^{1/2}\text{Pr}^{1/3}$	$\text{Pr} \geq 0.6$
$C_f = \frac{1.328}{\text{Re}_L^{1/2}}$	$\text{Pr} \geq 0.6$
$\text{Nu} = 0.664\text{Re}_L^{1/2}\text{Pr}^{1/3}$	$\text{Pr} \geq 0.6$
Turbulent flow over a flat plate:	
$C_f(x) = \frac{0.0592}{\text{Re}_x^{1/5}}$	$5 \times 10^5 \leq \text{Re}_x \leq 10^7$
$\text{Nu}(x) = 0.0296\text{Re}_x^{4/5}\text{Pr}^{1/3}$	$\begin{cases} 0.6 \leq \text{Pr} \leq 60 \\ 5 \times 10^5 \leq \text{Re}_x \leq 10^7 \end{cases}$
$C_f = \frac{0.074}{\text{Re}_L^{1/5}}$	$5 \times 10^5 \leq \text{Re}_L \leq 10^7$
$\text{Nu} = 0.037\text{Re}_L^{4/5}\text{Pr}^{1/3}$	$\begin{cases} 0.6 \leq \text{Pr} \leq 60 \\ 5 \times 10^5 \leq \text{Re}_x \leq 10^7 \end{cases}$
Mixed flow over a flat plate:	
$C_f(x) = \frac{0.074}{\text{Re}_L^{1/5}} - \frac{1742}{\text{Re}_L}$	$5 \times 10^5 \leq \text{Re}_L \leq 10^7$
$\text{Nu} = (0.037\text{Re}_L^{4/5} - 871)\text{Pr}^{1/3}$	$\begin{cases} 0.6 \leq \text{Pr} \leq 60 \\ 5 \times 10^5 \leq \text{Re}_x \leq 10^7 \end{cases}$
Flat plate with uniform heat flux:	
$\text{Nu}(x) = 0.453\text{Re}_x^{1/2}\text{Pr}^{1/3}$	Laminar flow
$\text{Nu}(x) = 0.0308\text{Re}_x^{0.8}\text{Pr}^{1/3}$	Turbulent flow
Fully developed laminar flow in a pipe:	
$\text{Nu} = 3.66$	Constant surface temperature
$\text{Nu} = 4.36$	Constant heat flux
Fully developed turbulent flow in a pipe:	
$\text{Nu}_D = 0.023\text{Re}_D^{4/5}\text{Pr}^n$	$\begin{cases} 0.7 \leq \text{Pr} \leq 160 \\ \text{Re} > 10000 \end{cases}$
$(n = 0.4 \text{ for heating, } n = 0.3 \text{ for cooling})$	

E.4 Continuity and equation of motion

E.4.1 Cylindrical polar coordinates

Equation of continuity for unsteady flow, variable density:

$$\frac{\partial \rho}{\partial t} + \frac{1}{r} \frac{\partial (r \rho v_r)}{\partial r} + \frac{1}{r} \frac{\partial (\rho v_\theta)}{\partial \theta} + \frac{\partial (\rho v_x)}{\partial x} = 0$$

Equations of Motion for unsteady flow, variable density: Cauchy form

$$\begin{aligned} \frac{\partial v_x}{\partial t} + v_x \frac{\partial v_x}{\partial x} + v_r \frac{\partial v_x}{\partial r} + \frac{v_\theta}{r} \frac{\partial v_x}{\partial \theta} &= -\frac{1}{\rho} \frac{\partial p}{\partial x} + F_{x,\text{int}} + F_{x,\text{ext}} \\ \frac{\partial v_r}{\partial t} + v_x \frac{\partial v_r}{\partial x} + v_r \frac{\partial v_r}{\partial r} + \frac{v_\theta}{r} \frac{\partial v_r}{\partial \theta} - \frac{v_\theta^2}{r} &= -\frac{1}{\rho} \frac{\partial p}{\partial r} + F_{r,\text{int}} + F_{r,\text{ext}} \\ \frac{\partial v_\theta}{\partial t} + v_x \frac{\partial v_\theta}{\partial x} + v_r \frac{\partial v_\theta}{\partial r} + \frac{v_\theta}{r} \frac{\partial v_\theta}{\partial \theta} + \frac{v_\theta v_r}{r} &= -\frac{1}{\rho r} \frac{\partial p}{\partial \theta} + F_{\theta,\text{int}} + F_{\theta,\text{ext}} \end{aligned}$$

where $F_{i,\left\{\begin{smallmatrix} \text{int} \\ \text{ext} \end{smallmatrix}\right\}}$ are the internal (viscous) or external (body) forces per unit mass, as appropriate, acting in the direction of coordinate i . For example,

$$F_{x,\text{int}} = \nu \left[\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial v_x}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 v_x}{\partial \theta^2} + \frac{\partial^2 v_x}{\partial x^2} \right]$$

E.4.2 Rectangular Cartesian coordinates

Equation of continuity for unsteady flow, variable density

$$\frac{\partial \rho}{\partial t} + \frac{\partial (\rho u)}{\partial x} + \frac{\partial (\rho v)}{\partial y} + \frac{\partial (\rho w)}{\partial z} = 0$$

Equations of motion for unsteady flow, variable density: Cauchy form

$$\begin{aligned} \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} &= -\frac{1}{\rho} \frac{\partial p}{\partial x} + F_{x,\text{int}} + F_{x,\text{ext}} \\ \frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} &= -\frac{1}{\rho} \frac{\partial p}{\partial y} + F_{y,\text{int}} + F_{y,\text{ext}} \\ \frac{\partial w}{\partial t} + u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z} &= -\frac{1}{\rho} \frac{\partial p}{\partial z} + F_{z,\text{int}} + F_{z,\text{ext}} \end{aligned}$$

Equations of motion for unsteady uniform property flow in two dimensions (the xy plane) only:

$$\begin{aligned} \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} &= -\frac{1}{\rho} \frac{\partial p}{\partial x} + \underbrace{\frac{\mu}{\rho} \left(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right)}_{F_{x,\text{int}}} + F_{x,\text{ext}} \\ \frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} &= -\frac{1}{\rho} \frac{\partial p}{\partial y} + \underbrace{\frac{\mu}{\rho} \left(\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} \right)}_{F_{y,\text{int}}} + F_{y,\text{ext}} \end{aligned}$$

The boundary layer (“approximately Couette flow”) form of the equations of motion for strain confined to the xy plane with uniform properties:

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = -\frac{1}{\rho} \frac{dp}{dx} + \frac{\mu}{\rho} \left(\frac{\partial^2 u}{\partial y^2} \right)$$

E.4.3 Vector form

Equation of continuity for unsteady flow, variable density, in vector form:

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{V}) = 0$$

where ∇ is the vector-gradient operator expressing the divergence of a vector, in this case \mathbf{V} , the velocity field.

Equations of Motion in vector form for unsteady flow: Cauchy form

$$\frac{\partial \mathbf{V}}{\partial t} + (\mathbf{V} \cdot \nabla) \frac{\partial \mathbf{V}}{\partial x} = -\frac{1}{\rho} \nabla p + \mathbf{F}_{\text{int}} + \mathbf{F}_{\text{ext}}$$

E.5 Equations for compressible flows

Isentropic compressible flow relations

$$\begin{aligned} \rho_0 &= \rho_1 \left(1 + \frac{\gamma - 1}{2} \text{Ma}_1^2 \right)^{\frac{1}{\gamma-1}} \\ \rho_0 &= \rho_1 \left(1 + \frac{\gamma - 1}{2} \text{Ma}_1^2 \right)^{\frac{\gamma}{\gamma-1}} \\ T_0 &= T_1 \left(1 + \frac{\gamma - 1}{2} \text{Ma}_1^2 \right) \\ a_0 &= a_1 \left(1 + \frac{\gamma - 1}{2} \text{Ma}_1^2 \right)^{1/2} \end{aligned}$$

Prantl-Meyer function

$$\nu(\text{Ma}) = \left(\frac{\gamma + 1}{\gamma - 1} \right)^{1/2} \tan^{-1} \left\{ \left(\frac{(\gamma + 1)(\text{Ma}^2 - 1)}{\gamma - 1} \right)^{1/2} \right\} - \tan^{-1} \left\{ (\text{Ma}^2 - 1)^{1/2} \right\}$$

Normal Shock Relations

$$\begin{aligned} \text{Ma}_2^2 &= \frac{1 + \frac{1}{2}(\gamma - 1) \text{Ma}_1^2}{\gamma \text{Ma}_1^2 - \frac{1}{2}(\gamma - 1)} \\ \frac{\rho_2}{\rho_1} &= \frac{(\gamma + 1) \text{Ma}_1^2}{(\gamma - 1) \text{Ma}_1^2 + 2} \end{aligned}$$

$$\frac{p_2}{p_1} = 1 + \frac{2\gamma}{(\gamma + 1)} (\text{Ma}_1^2 - 1)$$

$$\frac{T_2}{T_1} = \frac{\left[2\gamma \text{Ma}_1^2 - (\gamma - 1) \right] \left[(\gamma - 1) \text{Ma}_1^2 + 2 \right]}{(\gamma + 1)^2 \text{Ma}_1^2}$$

E.6 Friction factor for flow in circular pipes (Moody diagram)

d = pipe diameter

f = Darcy friction factor = $\frac{4\tau_w}{\frac{1}{2}\rho\bar{V}^2} = \frac{1}{(L/d)} \frac{\Delta P}{\frac{1}{2}\rho\bar{V}^2}$

L = pipe length

Re = Reynolds Number = $\frac{\rho\bar{V}d}{\mu}$

\bar{V} = fluid bulk mean velocity

ΔP = frictional pressure drop in length L

ε = roughness height

μ = absolute or dynamic viscosity

ρ = fluid density

τ_w = shear stress at pipe wall

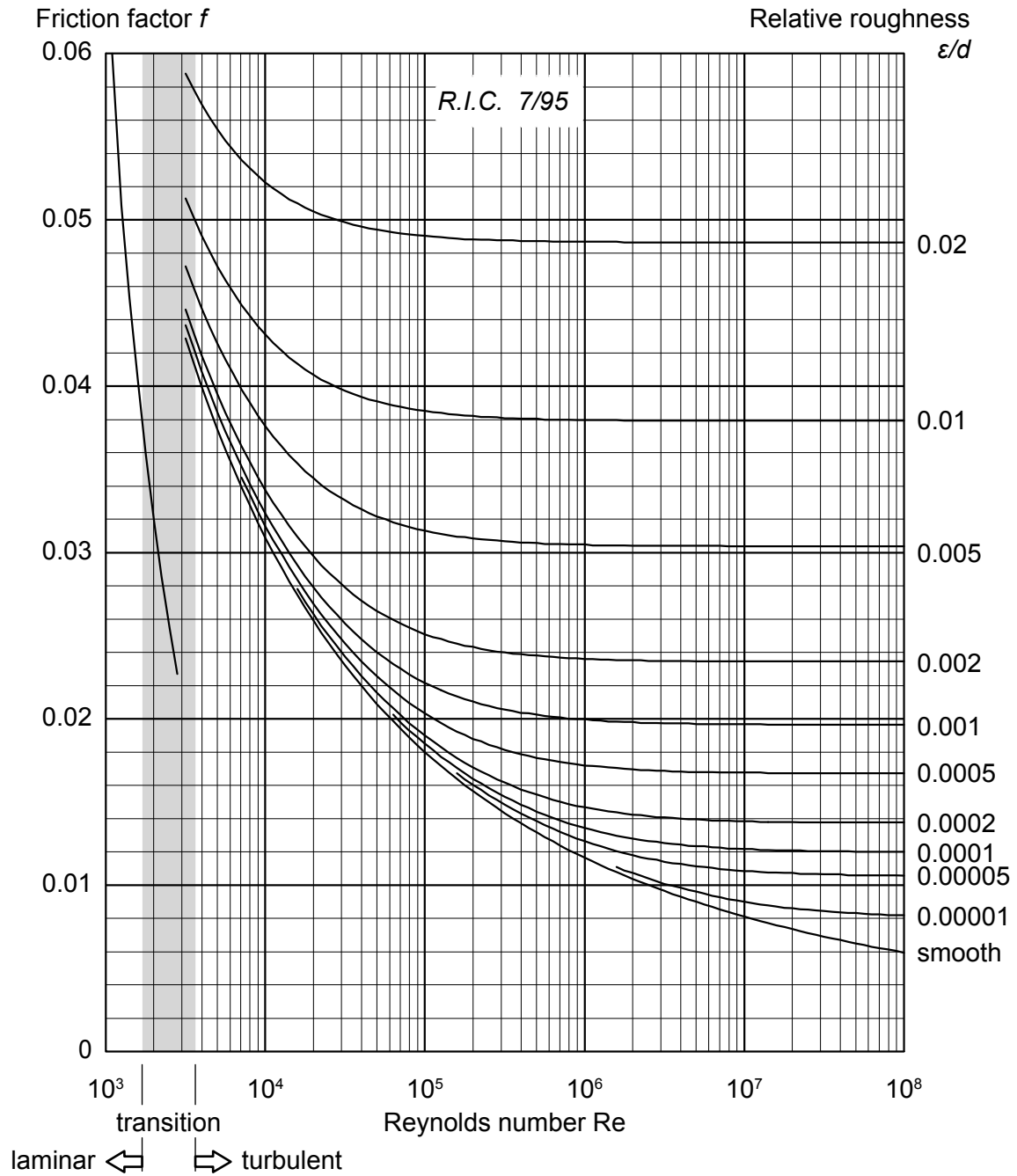


Figure E.1: Moody Diagram

E.7 Perfect gases

Ma	=	Mach number
P, P_0	=	absolute pressure, stagnation pressure
T, T_0	=	absolute temperature, stagnation temperature
v	=	specific volume
ρ, ρ_0	=	density, stagnation density

Over a limited range of temperatures and pressures close to ambient values, the following substances can be assumed to behave as *perfect* gases with properties given by the following relationships:

equation of state	$Pv = RT$
specific heat at constant volume	$C_v = \frac{du}{dT} = \text{constant for the particular gas}$
specific heat at constant pressure	$C_p = \frac{dh}{dT} = \text{constant for the particular gas}$
ratio of principal specific heats	$\gamma = \frac{C_p}{C_v} = \text{constant for the particular gas}$
gas constant	$R = C_p - C_v = \text{constant for the particular gas}$

and $R = \frac{\bar{R}}{M}$ where \bar{R} = universal gas constant = $8.314 \text{ kJ kmol}^{-1} \text{ K}^{-1}$.

Table E.3: Perfect gases (ideal gases with constant specific heats)

Gas	Chemical formula	Molar mass M kg kmol^{-1}	Gas constant R $\text{kJ kg}^{-1} \text{ K}^{-1}$	\bar{C}_p $\text{kJ kmol}^{-1} \text{ K}^{-1}$	\bar{C}_v $\text{kJ kmol}^{-1} \text{ K}^{-1}$	γ
air ^a	—	28.96	0.287	1.01	0.72	1.40
oxygen	O ₂	32.00	0.260	0.92	0.66	1.40
nitrogen	N ₂	28.01	0.297	1.04	0.74	1.40
atmospheric nitrogen ^b	(AN)	28.17	0.295	1.03	0.74	1.40
carbon dioxide	CO ₂	44.01	0.189	0.84	0.65	1.29
carbon monoxide	CO	28.01	0.297	1.04	0.74	1.40
hydrogen	H ₂	2.016	4.12	14.31	10.18	1.41
methane	CH ₄	16.04	0.518	2.23	1.71	1.30
ethane	C ₂ H ₆	30.07	0.277	1.75	1.47	1.19
helium	He	4.00	2.08	5.20	3.12	1.67

^aComposition of dry air: 21.0% oxygen, 79.0% atmospheric nitrogen by no. of kmol or by volume; 23.2% oxygen, 76.8% atmospheric nitrogen by mass.

^bAtmospheric nitrogen contains approx. 1% (by no. of kmol or volume) argon and traces of carbon dioxide and other gases, in addition to nitrogen

Table E.4: Isentropic compressible flow functions for perfect gas with $\gamma = 1.40$

Ma	$\frac{P}{P_0}$	$\frac{\rho}{\rho_0}$	$\frac{T}{T_0}$	Ma	$\frac{P}{P_0}$	$\frac{\rho}{\rho_0}$	$\frac{T}{T_0}$
0	1	1	1	1	0.5283	0.6339	0.8333
0.05	0.9983	0.9988	0.9995	1.02	0.5160	0.6234	0.8278
0.10	0.9930	0.9950	0.9980	1.04	0.5039	0.6129	0.8222
0.15	0.9844	0.9888	0.9955	1.06	0.4919	0.6024	0.8165
				1.08	0.4800	0.5920	0.8108
0.20	0.9725	0.9803	0.9921				
0.22	0.9668	0.9762	0.9904	1.10	0.4684	0.5817	0.8052
0.24	0.9607	0.9718	0.9886	1.15	0.4398	0.5562	0.7908
0.26	0.9541	0.9670	0.9867	1.20	0.4124	0.5311	0.7764
0.28	0.9470	0.9619	0.9846	1.25	0.3861	0.5067	0.7619
				1.30	0.3609	0.4829	0.7474
0.30	0.9395	0.9564	0.9823	1.35	0.3370	0.4598	0.7329
0.32	0.9315	0.9506	0.9799				
0.34	0.9231	0.9445	0.9774	1.40	0.3142	0.4374	0.7184
0.36	0.9143	0.9380	0.9747	1.45	0.2927	0.4158	0.7040
0.38	0.9052	0.9313	0.9719	1.50	0.2724	0.3950	0.6897
				1.55	0.2533	0.3750	0.6754
0.40	0.8956	0.9243	0.9690	1.60	0.2353	0.3557	0.6614
0.42	0.8857	0.9170	0.9659	1.65	0.2184	0.3373	0.6475
0.44	0.8755	0.9094	0.9627				
0.46	0.8650	0.9016	0.9594	1.70	0.2026	0.3197	0.6337
0.48	0.8541	0.8935	0.9559	1.75	0.1878	0.3029	0.6202
				1.80	0.1740	0.2868	0.6068
0.50	0.8430	0.8852	0.9524	1.85	0.1612	0.2715	0.5936
0.52	0.8317	0.8766	0.9487	1.90	0.1492	0.2570	0.5807
0.54	0.8201	0.8679	0.9449	1.95	0.1381	0.2432	0.5680
0.56	0.8082	0.8589	0.9410				
0.58	0.7962	0.8498	0.9370	2.00	0.1278	0.2300	0.5556
				2.10	0.1094	0.2058	0.5313
0.60	0.7840	0.8405	0.9328	2.20	0.09352	0.1841	0.5081
0.62	0.7716	0.8310	0.9286	2.30	0.07997	0.1646	0.4859
0.64	0.7591	0.8213	0.9243	2.40	0.06840	0.1472	0.4647
0.66	0.7465	0.8115	0.9199				
0.68	0.7338	0.8016	0.9153	2.50	0.05853	0.1317	0.4444
				2.60	0.05012	0.1179	0.4252
0.70	0.7209	0.7916	0.9107	2.70	0.04295	0.1056	0.4068
0.72	0.7080	0.7814	0.9061	2.80	0.03685	0.09463	0.3894
0.74	0.6951	0.7712	0.9013	2.90	0.03165	0.08489	0.3729
0.76	0.6821	0.7609	0.8964				
0.78	0.6691	0.7505	0.8915	3.00	0.02722	0.07623	0.3571
				3.20	0.02023	0.06165	0.3281
0.80	0.6560	0.7400	0.8865	3.40	0.01512	0.05009	0.3019
0.82	0.6430	0.7295	0.8815	3.60	0.01138	0.04089	0.2784
0.84	0.6300	0.7189	0.8763	3.80	0.008629	0.03355	0.2572
0.86	0.6170	0.7083	0.8711				
0.88	0.6041	0.6977	0.8659	4.00	0.006586	0.02766	0.2381
				4.50	0.003455	0.01745	0.1980
0.90	0.5913	0.6870	0.8606	5.00	0.001890	0.01134	0.1667
0.92	0.5785	0.6764	0.8552				
0.94	0.5658	0.6658	0.8498	6.00	0.000633	0.005194	0.1220
0.96	0.5532	0.6551	0.8444	8.00	0.000102	0.001414	0.07246
0.98	0.5407	0.6445	0.8389	10.00	0.000024	0.000495	0.04762
1	0.5283	0.6339	0.8333	∞	0	0	0

Table E.5: Ideal (semi-perfect) gas specific enthalpy h (kJ kg^{-1} , 25°C datum)
for combustion calculations on a mass basis

T ($^\circ\text{C}$)	carbon dioxide CO_2	water vapour H_2O	nitrogen N_2	atmos. nitrogen (AN)	oxygen O_2	air —	carbon monoxide CO	hydrogen H_2
0	−22.5	−45.7	−25.6	−25.4	−23.1	−24.8	−25.7	−356.8
25	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
100	69.2	139.5	77.5	76.8	70.1	75.2	77.9	1074.5
200	165.3	331.0	182.4	180.9	165.5	177.2	183.5	2517.0
300	266.0	528.9	289.3	286.8	263.1	281.2	291.2	3970.5
400	371.1	733.1	398.0	394.6	362.9	387.1	400.9	5435.3
500	480.7	943.6	508.6	504.3	465.0	494.9	512.7	6911.1
600	594.8	1160.5	621.1	615.8	569.2	604.7	626.5	8398.1
700	713.3	1383.8	735.4	729.2	675.6	716.4	742.5	9896.3
800	836.4	1613.3	851.6	844.4	784.2	830.0	860.4	11405.5
900	963.9	1849.2	969.8	961.5	895.0	945.6	980.5	12925.9
1000	1095.9	2091.5	1089.8	1080.4	1008.0	1063.2	1102.6	14457.5
1100	1232.3	2340.1	1211.6	1201.2	1123.2	1182.6	1226.7	16000.2
1200	1373.3	2595.0	1335.4	1323.9	1240.6	1304.0	1352.9	17554.0
1300	1518.7	2856.3	1461.0	1448.4	1360.2	1427.4	1481.2	19119.0
1400	1668.7	3123.9	1588.5	1574.8	1482.0	1552.7	1611.6	20695.1
1500	1823.1	3397.8	1717.9	1703.1	1606.0	1679.9	1744.0	22282.4

Enthalpy values in Table E.5 have been computed using the approximation

$$C_p = a + bT$$

so that

$$h - h_D = \int C_p dT = (T - T_D) \left[a + \frac{1}{2}b(T + T_D) \right]$$

where datum temperature $T_D = 298.15 \text{ K}$ and datum enthalpy h_D (at $T = T_D$) = 0 (this is equivalent to using a mean C_p between 298.15 K (25°C) and T). The values of the constants are tabulated below; T must be in K, giving h in kJ kg^{-1} . The magnitudes of the maximum and mean errors in h refer to the range 0 to 1500°C .

	carbon dioxide CO_2	water vapour H_2O	nitrogen N_2	atmos. nitrogen (AN)	oxygen O_2	air —	carbon monoxide CO	hydrogen H_2
a	0.772	1.647	0.970	0.962	0.861	0.938	0.969	13.95
$b \times 10^6$ ($\text{kJ kg}^{-1} \text{K}^{-2}$)	448	634	188	186	220	194	206	1114
max. error	4.0	0.7	0.5	0.6	1.3	0.4	0.5	0.7
mean. error (%)	1.4	0.2	0.2	0.2	0.5	0.2	0.2	0.3

Table E.6: Molar Enthalpy of Formation h_f^0 (kJ kmol⁻¹ at 25 °C and 1 atmosphere) as gas or vapour (g), except where indicated as solid (s) or liquid (l).

carbon as graphite	C(s)	0
hydrogen	H ₂	0
methane	CH ₄	-74 850
ethane	C ₂ H ₆	-84 680
propane	C ₃ H ₈	-103 850
n-octane	C ₈ H ₁₈ (l)	-249 950
ethanol	C ₂ H ₅ OH(l)	-277 690
hydrogen peroxide	H ₂ O ₂	-136 310
carbon dioxide	CO ₂	-393 520
water vapour	H ₂ O(g)	-241 820
liquid water	H ₂ O(l)	-285 830
nitrogen	N ₂	0
atmospheric nitrogen	(AN)	0
oxygen	O ₂	0
air	—	0
carbon monoxide	CO	-110 530

Table E.7: Ideal gas molar enthalpy h (kJ kmol⁻¹, 25 °C datum)

T (°C)	carbon dioxide CO ₂	water vapour H ₂ O	nitrogen N ₂	atmos. nitrogen (AN)	oxygen O ₂	air ^a —	carbon monoxide CO	hydrogen H ₂
0	-990	-823	-717	-715	-739	-719	-720	-719
25	0	0	0	0	0	0	0	0
100	3 045	2 513	2 170	2 164	2 244	2 179	2 181	2 166
200	7 276	5 964	5 110	5 096	5 297	5 133	5 139	5 074
300	11 705	9 528	8 103	8 080	8 420	8 143	8 155	8 005
400	16 332	13 207	11 148	11 117	11 614	11 210	11 229	10 957
500	21 155	17 001	14 245	14 205	14 878	14 333	14 360	13 933
600	26 176	20 908	17 396	17 347	18 213	17 512	17 550	16 931
700	31 393	24 930	20 599	20 540	21 618	20 747	20 796	19 951
800	36 808	29 066	23 855	23 786	25 094	24 038	24 101	22 994
900	42 420	33 316	27 163	27 085	28 640	27 385	27 463	26 059
1000	48 229	37 680	30 524	30 436	32 256	30 789	30 883	29 146
1100	54 236	42 159	33 938	33 839	35 943	34 249	34 361	32 256
1200	60 439	46 751	37 404	37 295	39 700	37 765	37 896	35 389
1300	66 840	51 458	40 923	40 803	43 527	41 337	41 489	38 544
1400	73 438	56 280	44 495	44 363	47 425	44 965	45 140	41 721
1500	80 233	61 215	48 119	47 976	51 393	48 650	48 848	44 921

^aN.B. In a reaction equation, $n_{\text{ox}}(\text{O}_2 + 3.762\text{N}_2)$ represents $4.762n_{\text{ox}}$ equivalent kmol of air

E.8 Heating (or calorific) values of fuels M = molar mass $\overline{C_p}$ = mean constant-pressure specific heat for use near 25 °C Abbreviations: $\overline{\rho}$ = approximate density

GCV gross calorific value (= HHV = HCV)

HHV higher heating value (=GCV = HCV = negative of enthalpy of combustion with liquid H₂O in products)LHV lower heating value (=NCV = LCV = negative of enthalpy of combustion with vapour H₂O in products)

NCV net calorific value (=LHV = LCV)

Table E.8: Heating (or calorific) values of gas fuels at 25 °C.

Gas	M kg kmol ⁻¹	HHV or GCV kJ kg ⁻¹	LHV or NCV kJ kg ⁻¹	$\overline{C_p}$ kJ kg ⁻¹ K ⁻¹
hydrogen	2.016	141 800	119 980	14.31
methane	16.04	55 500	50 020	2.23
ethane	30.07	51 880	47 490	1.75
propane	44.10	50 350	46 360	1.67
n-butane	58.12	49 500	45 720	1.68
n-pentane	72.15	49 020	45 360	1.67
n-hexane	86.18	48 680	45 110	1.66
carbon monoxide	28.01	10 100	10 100	1.04
typical North Sea gas ^a	17.05	53 510	48 290	2.15

^amolar composition: CH₄ 94.4%, C₂H₆ 3.0%, N₂ 1.5%, other gases 1.1%. Elemental composition by mass: C 73.26%, H 23.90%, O 0.38%, N 2.46%.

Table E.9: Heating (or calorific) values of liquid fuels at 25 °C.

Liquid	Approx. elemental composition by mass (%)	$\overline{\rho}$ kg m ⁻³	HHV or GCV kJ kg ⁻¹	LHV or NCV kJ kg ⁻¹	$\overline{C_p}$ kJ kg ⁻¹ K ⁻¹
n-octane C ₈ H ₁₈	C84.1 H15.9	703	47 890	44 420	2.11
methanol CH ₃ OH	C37.5 H12.6 O49.9	790	22 690	19 960	2.51
petrol (gasoline)	C85.0 H15.0	740	46 900	43 630	2.06
kerosine	C86.1 H13.9	770	46 140	43 100	2.02
distillate fuel oil	C86.8 H13.2	820	45 600	42 720	1.95

E.9 Properties of R134a refrigerant

R134a or HFC134a is a hydrofluorocarbon refrigerant (1,1,1,2-tetrafluoroethane, CH_2FCF_3) with zero ozone-depleting potential, although it has some global warming potential. It is a substitute for the chlorofluorocarbon refrigerant R12 (banned under the Montreal Protocol 1984) in domestic refrigeration and freezing applications and in the coolers of air conditioning plant.

T, T_{sat}	=	temperature, at saturation
P	=	absolute pressure
v	=	specific volume, $\text{m}^3 \text{kg}^{-1}$
h	=	specific enthalpy, kJ kg^{-1}
s	=	specific entropy, $\text{kJ kg}^{-1} \text{K}^{-1}$

Table E.10: Saturated Refrigerant 134a — Temperature (−60°C to critical point)

T (°C)	P bar (abs)	v_f $\text{m}^3 \text{kg}^{-1}$	v_g $\text{m}^3 \text{kg}^{-1}$	h_f kJ kg^{-1}	h_g kJ kg^{-1}	s_f $\text{kJ kg}^{-1} \text{K}^{-1}$	s_g $\text{kJ kg}^{-1} \text{K}^{-1}$
−60	0.1587	0.0006795	1.0808	22.92	261.17	0.6828	1.8005
−50	0.2942	0.0006923	0.6064	35.33	267.44	0.7396	1.7798
−40	0.5118	0.0007060	0.3609	47.88	273.71	0.7946	1.7632
−35	0.6612	0.0007132	0.2838	54.22	276.84	0.8214	1.7562
−30	0.8436	0.0007206	0.2257	60.60	279.95	0.8479	1.7500
−25	1.064	0.0007284	0.1814	67.03	283.05	0.8740	1.7445
−20	1.327	0.0007364	0.1473	73.51	286.13	0.8998	1.7397
−15	1.639	0.0007448	0.1206	80.05	289.18	0.9252	1.7354
−10	2.005	0.0007536	0.09954	88.64	292.20	0.9504	1.7316
−5	2.432	0.0007627	0.08279	93.29	295.19	0.9753	1.7283
0	2.925	0.0007723	0.06933	100.00	298.10	1.0000	1.7254
5	3.492	0.0007823	0.05842	106.78	301.02	1.0244	1.7228
10	4.139	0.0007929	0.04951	113.62	303.86	1.0486	1.7205
15	4.873	0.0008041	0.04218	120.54	306.64	1.0727	1.7185
20	5.702	0.0008160	0.03610	127.54	309.35	1.0965	1.7167
25	6.634	0.0008285	0.03102	134.61	311.97	1.1202	1.7150
30	7.675	0.0008419	0.02676	141.77	314.49	1.1437	1.7134
35	8.835	0.0008563	0.02315	149.02	316.91	1.1671	1.7119
40	10.12	0.0008718	0.02008	156.37	319.20	1.1904	1.7104
45	11.55	0.0008886	0.01746	163.83	321.34	1.2136	1.7087
50	13.11	0.0009068	0.01520	171.41	323.31	1.2368	1.7069
60	16.73	0.0009493	0.01154	187.00	326.60	1.2833	1.7024
80	26.21	0.001077	0.006516	221.07	328.95	1.3798	1.6852
101	40.55	0.001964	0.001964	289.40	289.40	1.5609	1.5609

Table E.11: Saturated Refrigerant 134a — Pressure (0.2 bar to critical point)

P bar (abs)	T °C	v_f $\text{m}^3 \text{kg}^{-1}$	v_g $\text{m}^3 \text{kg}^{-1}$	h_f kJ kg^{-1}	h_g kJ kg^{-1}	s_f $\text{kJ kg}^{-1} \text{K}^{-1}$	s_g $\text{kJ kg}^{-1} \text{K}^{-1}$
0.2	−56.38	0.0006841	0.8703	27.40	263.44	0.7035	1.7925
0.4	−44.58	0.0006996	0.4547	42.11	270.84	0.7696	1.7703
0.6	−36.93	0.0007104	0.3109	51.77	275.64	0.8111	1.7588
0.8	−31.11	0.0007189	0.2373	59.18	279.26	0.8420	1.7513
1.0	−26.36	0.0007262	0.1923	65.28	282.21	0.8669	1.7460
1.2	−22.31	0.0007327	0.1620	70.51	284.71	0.8879	1.7418
1.4	−18.75	0.0007385	0.1400	75.14	286.89	0.9062	1.7385
1.6	−15.58	0.0007438	0.1234	79.29	288.83	0.9223	1.7358
2.0	−10.06	0.0007534	0.09978	86.53	292.16	0.9500	1.7316
2.5	−4.26	0.0007641	0.08062	94.28	295.62	0.9790	1.7278
3.0	0.70	0.0007737	0.06766	100.95	298.54	1.0034	1.7250
3.5	5.07	0.0007825	0.05829	106.87	301.06	1.0247	1.7228
4.0	8.98	0.0007907	0.05119	112.22	303.29	1.0437	1.7210
5.0	15.80	0.0008060	0.04113	121.66	307.08	1.0765	1.7182
6.0	21.66	0.0008201	0.03431	129.88	310.23	1.1044	1.7161
8.0	31.45	0.0008460	0.02565	143.86	315.21	1.1505	1.7130
10.0	39.55	0.0008703	0.02034	155.70	319.00	1.1883	1.7105
12.0	46.50	0.0008939	0.01675	166.09	321.95	1.2206	1.7082
15.0	55.45	0.0009289	0.01308	179.83	325.23	1.2621	1.7046
20.0	67.72	0.0009896	0.009318	199.58	328.37	1.3197	1.6975
30.0	86.38	0.001144	0.005306	233.52	327.42	1.4135	1.6747
40.55	101.00	0.001964	0.001964	289.35	289.35	1.5609	1.5609

Table E.12: Superheated Refrigerant 134a (0.2 bar to 1 bar)

T (°C)	0.2 bar abs ($T_{\text{sat}} = -56.38\text{ °C}$)			0.4 bar abs ($T_{\text{sat}} = -44.58\text{ °C}$)			0.6 bar abs ($T_{\text{sat}} = -36.93\text{ °C}$)			0.8 bar abs ($T_{\text{sat}} = -31.11\text{ °C}$)			1.0 bar abs ($T_{\text{sat}} = -26.36\text{ °C}$)			T (°C)
	v	h	s	v	h	s	v	h	s	v	h	s	v	h	s	
Sat.	0.8703	263.44	1.7925	0.4547	270.84	1.7703	0.3109	275.64	1.7588	0.2373	279.26	1.7513	0.1923	282.21	1.7460	Sat.
-50	0.8975	267.92	1.8129	0.4647	274.21	1.7849										-50
-40	0.9398	275.08	1.8443	0.4864	281.67	1.8162	0.3212	280.90	1.7808	0.2386	280.13	1.7549				-40
-30	0.9818	282.41	1.8750	0.5079	289.27	1.8469	0.3359	288.61	1.8119	0.2499	287.95	1.7864	0.1982	287.27	1.7662	-30
-20	1.0236	289.91	1.9053	0.5291	297.03	1.8769	0.3504	296.46	1.8422	0.2610	295.88	1.8171	0.2073	295.30	1.7973	-20
-10	1.0652	297.59	1.9350				0.3647	304.45	1.8720	0.2719	303.94	1.8472				-10
0	1.107	305.43	1.9643	0.5502	304.94	1.9064							0.2162	303.43	1.8276	0
10	1.148	313.45	1.9931	0.5712	313.02	1.9355	0.3789	312.58	1.9013	0.2827	312.14	1.8767	0.2250	311.69	1.8573	10
20	1.189	321.64	2.0215	0.5921	321.26	1.9641	0.3930	320.87	1.9300	0.2935	320.47	1.9056	0.2337	320.08	1.8864	20
30	1.231	330.01	2.0496	0.6129	329.66	1.9922	0.4071	329.31	1.9584	0.3041	328.96	1.9341	0.2423	328.60	1.9150	30
40	1.272	338.54	2.0773	0.6337	338.22	2.0200	0.4210	337.91	1.9863	0.3147	337.59	1.9621	0.2509	337.27	1.9432	40
50				0.6544	346.95	2.0475	0.4350	346.67	2.0138	0.3252	346.38	1.9897	0.2594	346.09	1.9709	50
60				0.6751	355.84	2.0746	0.4489	355.58	2.0410	0.3357	355.32	2.0169	0.2679	355.05	1.9982	60
70							0.4627	364.66	2.0678	0.3462	364.41	2.0438	0.2763	364.17	2.0251	70
80													0.2847	373.44	2.0518	80

Table E.13: Superheated Refrigerant 134a (1.5 bar to 4 bar)

T(°C)	1.5 bar abs ($T_{\text{sat}} = -17.13\text{ °C}$)			2.0 bar abs ($T_{\text{sat}} = -10.06\text{ °C}$)			2.5 bar abs ($T_{\text{sat}} = -4.26\text{ °C}$)			3.0 bar abs ($T_{\text{sat}} = 0.70\text{ °C}$)			3.5 bar abs ($T_{\text{sat}} = 8.98\text{ °C}$)			T(°C)
	v	h	s	v	h	s	v	h	s	v	h	s	v	h	s	
Sat.	0.1311	287.89	1.7371	0.0998	292.16	1.7316	0.0806	295.62	1.7278	0.0677	298.54	1.7250	0.0512	303.29	1.7210	Sat.
-10	0.1357	293.79	1.7599	0.0998	292.22	1.7318										-10
0	0.1419	302.13	1.7910	0.1047	300.77	1.7638	0.0824	299.37	1.7416							0
10	0.1481	310.55	1.8212	0.1095	309.37	1.7947	0.0864	308.15	1.7732	0.0709	306.90	1.7550	0.0515	304.25	1.7244	10
20	0.1541	319.07	1.8508	0.1142	318.03	1.8247	0.0902	316.97	1.8038	0.0742	315.88	1.7862	0.0542	313.59	1.7568	20
30	0.1600	327.70	1.8798	0.1187	326.78	1.8541	0.0940	325.84	1.8336	0.0775	324.88	1.8164	0.0568	322.89	1.7880	30
40	0.1658	336.46	1.9082	0.1232	335.64	1.8828	0.0977	334.80	1.8627	0.0806	333.95	1.8458	0.0593	332.18	1.8181	40
50	0.1716	345.36	1.9362	0.1277	344.61	1.9110	0.1013	343.86	1.8911	0.0837	343.09	1.8745	0.0617	341.51	1.8475	50
60	0.1773	354.39	1.9637	0.1321	353.71	1.9388	0.1049	353.03	1.9191	0.0868	352.33	1.9027	0.0641	350.91	1.8761	60
70	0.1831	363.56	1.9908	0.1364	362.94	1.9661	0.1085	362.31	1.9465	0.0898	361.68	1.9303	0.0665	360.38	1.9041	70
80	0.1887	372.87	2.0176	0.1408	372.30	1.9930	0.1120	371.73	1.9736	0.0928	371.14	1.9575	0.0688	369.96	1.9316	80
90	0.1944	382.34	2.0440	0.1451	381.81	2.0195	0.1155	381.27	2.0002	0.0957	380.73	1.9843	0.0710	379.64	1.9586	90
100	0.2000	391.95	2.0701	0.1493	391.45	2.0457	0.1189	390.95	2.0265	0.0986	390.45	2.0107	0.0733	389.44	1.9853	100
110				0.1536	401.24	2.0716	0.1224	400.77	2.0525	0.1015	400.31	2.0368	0.0755	399.36	2.0115	110
120							0.1044	410.30	2.0625				0.0777	409.41	2.0374	120
130													0.0799	419.59	2.0630	130

Table E.14: Superheated Refrigerant 134a (5 bar to 12 bar)

T(°C)	5 bar abs ($T_{\text{sat}} = 15.80\text{ °C}$)			6 bar abs ($T_{\text{sat}} = 21.66\text{ °C}$)			8 bar abs ($T_{\text{sat}} = 31.45\text{ °C}$)			10 bar abs ($T_{\text{sat}} = 39.55\text{ °C}$)			12 bar abs ($T_{\text{sat}} = 46.50\text{ °C}$)			T(°C)
	v	h	s	v	h	s	v	h	s	v	h	s	v	h	s	
Sat.	0.0411	307.08	1.7182	0.0343	310.23	1.7161	0.0256	315.21	1.7130	0.0203	319.00	1.7105	0.0167	321.95	1.7082	Sat.
20	0.0421	311.16	1.7322													20
30	0.0443	320.79	1.7645	0.0360	318.56	1.7440										30
40	0.0465	330.34	1.7955	0.0379	328.41	1.7760	0.0270	324.24	1.7422	0.0204	319.51	1.7121				40
50	0.0485	339.88	1.8255	0.0397	338.18	1.8067	0.0286	334.56	1.7747	0.0218	330.58	1.7469	0.0172	326.10	1.7211	50
60	0.0505	349.44	1.8546	0.0414	347.93	1.8364	0.0300	344.74	1.8057	0.0231	341.30	1.7796	0.0184	337.53	1.7559	60
70	0.0524	359.06	1.8831	0.0431	357.69	1.8653	0.0314	354.85	1.8356	0.0243	351.82	1.8107	0.0195	348.56	1.7886	70
80	0.0543	368.75	1.9109	0.0447	367.51	1.8935	0.0327	364.94	1.8646	0.0254	362.23	1.8406	0.0205	359.36	1.8196	80
90	0.0562	378.53	1.9382	0.0463	377.39	1.9210	0.0339	375.05	1.8928	0.0265	372.60	1.8696	0.0215	370.04	1.8494	90
100	0.0581	388.41	1.9651	0.0479	387.36	1.9481	0.0352	385.21	1.9204	0.0276	382.97	1.8978	0.0224	380.65	1.8782	100
110	0.0599	398.40	1.9915	0.0495	397.42	1.9747	0.0364	395.43	1.9475	0.0286	393.38	1.9253	0.0234	391.26	1.9063	110
120	0.0617	408.51	2.0175	0.0510	407.60	2.0010	0.0376	405.75	1.9740	0.0296	403.84	1.9522	0.0242	401.89	1.9337	120
130	0.0635	418.74	2.0432	0.0525	417.89	2.0268	0.0388	416.15	2.0002	0.0306	414.38	1.9787	0.0251	412.57	1.9605	130
140	0.0653	429.11	2.0686	0.0540	428.30	2.0523	0.0400	426.67	2.0259	0.0316	425.01	2.0048	0.0259	423.32	1.9868	140
150							0.0412	437.30	2.0514	0.0325	435.73	2.0304	0.0268	434.15	2.0127	150

Table E.15: Superheated Refrigerant 134a (16 bar to 30 bar)

T (°C)	15 bar abs ($T_{\text{sat}} = 55.45\text{ °C}$)			18 bar abs ($T_{\text{sat}} = 63.13\text{ °C}$)			22 bar abs ($T_{\text{sat}} = 71.96\text{ °C}$)			26 bar abs ($T_{\text{sat}} = 79.62\text{ °C}$)			30 bar abs ($T_{\text{sat}} = 86.38\text{ °C}$)			T (°C)
	v	h	s	v	h	s	v	h	s	v	h	s	v	h	s	
Sat.	0.0131	325.23	1.7046	0.0106	327.42	1.7006	0.00826	328.95	1.6941	0.00659	328.99	1.6858	0.00531	327.42	1.6747	Sat.
60	0.0136	331.03	1.7222	0.0113	336.80	1.7282	0.00909	341.13	1.7290	0.00664	329.72	1.6878				60
70	0.0147	343.14	1.7580	0.0123	349.46	1.7646	0.00993	354.66	1.7668	0.00763	346.45	1.7346				70
80	0.0156	354.70	1.7912	0.0131	361.45	1.7981	0.0107	367.28	1.8011	0.00840	360.68	1.7732	0.00575	335.43	1.6969	80
90	0.0165	365.94	1.8225	0.0139	373.05	1.8296	0.0113	379.37	1.8331	0.00905	373.80	1.8079	0.00665	352.83	1.7442	90
100	0.0173	376.99	1.8526	0.0146	384.42	1.8596	0.0120	391.17	1.8634	0.00965	386.31	1.8402	0.00734	367.52	1.7830	100
110	0.0181	387.94	1.8815	0.0153	395.67	1.8886	0.0125	402.78	1.8926	0.0102	398.45	1.8707	0.00793	381.00	1.8178	110
120	0.0189	398.85	1.9096	0.0159	406.85	1.9167	0.0131	414.30	1.9208	0.0107	410.38	1.8999	0.00846	393.83	1.8500	120
130	0.0196	409.76	1.9371	0.0165	418.02	1.9441	0.0136	425.77	1.9483	0.0112	422.19	1.9281	0.00894	406.27	1.8805	130
140	0.0203	420.71	1.9639	0.0171	429.21	1.9708							0.00940	418.47	1.9096	140
150	0.0210	431.71	1.9902													150

E.10 Transport properties of air, water and steam

C_p	= specific heat at constant pressure	$\text{kJ kg}^{-1} \text{K}^{-1}$
C_v	= specific heat at constant volume	$\text{kJ kg}^{-1} \text{K}^{-1}$
k	= thermal conductivity	$\text{W m}^{-1} \text{K}^{-1}$
T	= temperature	K or $^{\circ}\text{C}$
x	= definition	$\text{kJ kg}^{-1} \text{K}^{-1}$
x	= definition	$\text{kJ kg}^{-1} \text{K}^{-1}$
α	= thermal diffusivity	$\text{m}^2 \text{s}^{-1}$
μ	= absolute viscosity	$\text{kg m}^{-1} \text{s}^{-1}$ (= N s m^{-2})
ν	= kinematic viscosity	$\text{m}^2 \text{s}^{-1}$
ρ	= density	kg m^{-3}

Table E.16: Transport properties of dry air at atmospheric pressure

Temperature T (°C)	Density ρ (kg m ⁻³)	Specific heat at constant pressure C_p (J kg ⁻¹ K ⁻¹)	Absolute (or dynamic) viscosity μ (kg m ⁻¹ s ⁻¹)	Kinematic viscosity $\nu = \frac{\mu}{\rho}$ (m ² s ⁻¹)	Thermal conductivity k (W m ⁻¹ K ⁻¹)	Thermal diffusivity α (m ² s ⁻¹)	Prandtl number $Pr = \frac{\mu C_p}{k}$	Temperature	
								$\frac{g\beta}{\alpha\nu} = \frac{GrPr}{L^3\Delta T}$ (m ⁻³ K ⁻¹)	T (°C)
-180	3.72	1035	6.50×10^{-6}	1.75×10^{-6}	0.0076	1.9×10^{-6}	0.92	3.2×10^{10}	-180
-100	2.04	1010	1.16×10^{-5}	5.69×10^{-6}	0.016	7.6×10^{-6}	0.75	1.3×10^9	-100
-50	1.582	1006	1.45×10^{-5}	9.17×10^{-6}	0.020	1.30×10^{-5}	0.72	3.67×10^8	-50
0	1.293	1006	1.71×10^{-5}	1.32×10^{-5}	0.024	1.84×10^{-5}	0.72	1.48×10^8	0
10	1.247	1006	1.76×10^{-5}	1.41×10^{-5}	0.025	1.96×10^{-5}	0.72	1.25×10^8	10
20	1.205	1006	1.81×10^{-5}	1.50×10^{-5}	0.025	2.08×10^{-5}	0.72	1.07×10^8	20
30	1.165	1006	1.86×10^{-5}	1.60×10^{-5}	0.026	2.23×10^{-5}	0.72	9.07×10^7	30
60	1.060	1008	2.00×10^{-5}	1.89×10^{-5}	0.028	2.74×10^{-5}	0.70	5.71×10^7	60
100	0.946	1011	2.18×10^{-5}	2.30×10^{-5}	0.032	3.28×10^{-5}	0.70	3.48×10^7	100
200	0.746	1025	2.58×10^{-5}	3.46×10^{-5}	0.039	5.19×10^{-5}	0.68	9.53×10^6	200
300	0.616	1045	2.95×10^{-5}	4.79×10^{-5}	0.045	7.17×10^{-5}	0.68	4.96×10^6	300
500	0.456	1093	3.58×10^{-5}	7.85×10^{-5}	0.056	1.14×10^{-4}	0.70	1.42×10^6	500
1000	0.277	1185	4.82×10^{-5}	1.74×10^{-4}	0.076	2.42×10^{-4}	0.72	1.8×10^5	1000

Table E.17: Transport properties of saturated water and steam

Temp. T (°C)	Specific volume		Specific heat at		Thermal		Absolute (or dynamic)		Prandtl number		Temp. T (°C)
	v_f (m ³ kg ⁻¹)	v_g (m ³ kg ⁻¹)	constant pressure C_{pf} (J kg ⁻¹ K ⁻¹)	C_{pg} (J kg ⁻¹ K ⁻¹)	k_f (W m ⁻¹ K ⁻¹)	conductivity k_g (W m ⁻¹ K ⁻¹)	μ_f (kg m ⁻¹ s ⁻¹)	viscosity μ_g (kg m ⁻¹ s ⁻¹)	Pr_f	Pr_g	
0.01	0.001000	206.0	4217	1854	0.569	0.0173	1.755×10^{-3}	8.8×10^{-6}	13.02	0.942	0.01
10	0.001000	106.3	4193	1860	0.587	0.0185	1.301×10^{-3}	9.1×10^{-6}	9.29	0.915	10
20	0.001002	57.78	4182	1866	0.603	0.0191	1.002×10^{-3}	9.4×10^{-6}	6.95	0.918	20
30	0.001004	32.90	4179	1875	0.618	0.0198	7.97×10^{-4}	9.7×10^{-6}	5.39	0.923	30
40	0.001008	19.53	4179	1885	0.632	0.0204	6.51×10^{-4}	1.01×10^{-5}	4.31	0.930	40
50	0.001012	12.04	4181	1899	0.643	0.0210	5.44×10^{-4}	1.04×10^{-5}	3.53	0.939	50
60	0.001017	7.674	4185	1915	0.653	0.0217	4.62×10^{-4}	1.07×10^{-5}	2.96	0.947	60
70	0.001023	5.045	4190	1936	0.662	0.0224	4.00×10^{-4}	1.11×10^{-5}	2.53	0.956	70
80	0.001029	3.409	4197	1962	0.670	0.0231	3.50×10^{-4}	1.14×10^{-5}	2.19	0.966	80
90	0.001036	2.362	4205	1992	0.676	0.0240	3.11×10^{-4}	1.17×10^{-5}	1.93	0.976	90
100	0.001043	1.674	4216	2028	0.681	0.0249	2.78×10^{-4}	1.21×10^{-5}	1.723	0.986	100
125	0.001065	0.7709	4254	2147	0.687	0.0272	2.19×10^{-4}	1.33×10^{-5}	1.358	1.047	125
150	0.001090	0.3929	4310	2314	0.687	0.0300	1.80×10^{-4}	1.44×10^{-5}	1.133	1.110	150
175	0.001121	0.2168	4389	2542	0.679	0.0334	1.53×10^{-4}	1.56×10^{-5}	0.990	1.185	175
200	0.001156	0.1273	4497	2843	0.665	0.0375	1.33×10^{-4}	1.67×10^{-5}	0.902	1.270	200
225	0.001199	0.07846	4648	3238	0.644	0.0427	1.182×10^{-4}	1.79×10^{-5}	0.853	1.36	225
250	0.001251	0.05011	4867	3772	0.616	0.0495	1.065×10^{-4}	1.91×10^{-5}	0.841	1.45	250
275	0.001317	0.03278	5202	4561	0.582	0.0587	9.72×10^{-5}	2.02×10^{-5}	0.869	1.56	275
300	0.001404	0.02167	5762	5863	0.541	0.0719	8.97×10^{-5}	2.14×10^{-5}	0.955	1.74	300
325	0.001528	0.01419	6861	8440	0.493	0.0929	7.90×10^{-5}	2.30×10^{-5}	1.100	2.09	325
350	0.001740	0.008812	10100	17150	0.437	0.1343	6.48×10^{-5}	2.58×10^{-5}	1.50	3.29	350
360	0.001894	0.006962	14600	25100	0.400	0.168	5.82×10^{-5}	2.75×10^{-5}	2.11	3.89	360
374	0.003106	0.003106	∞	∞	0.24	0.24	4.5×10^{-5}	4.5×10^{-5}	∞	∞	374

E.11 Approximate physical properties

ρ	= density	kg m^{-3}
C_p	= specific heat at constant pressure	$\text{J kg}^{-1} \text{K}^{-1}$
k	= thermal conductivity	$\text{W m}^{-1} \text{K}^{-1}$
μ	= absolute or dynamic viscosity	$\text{kg m}^{-1} \text{s}^{-1}$ or N s m^{-2}
σ	= surface tension	N m^{-1}

Table E.18: Approximate physical properties at 20 °C, 1 bar.

Gases ^a	ρ	C_p	k	μ	
air	1.19	1 010	0.025	1.81×10^{-5}	
oxygen	1.31	910	0.026	2.03×10^{-5}	
nitrogen	1.15	1 040	0.026	1.76×10^{-5}	
carbon dioxide	1.80	8 40	0.017	1.47×10^{-5}	
hydrogen	0.083	14 300	0.18	0.88×10^{-5}	
helium	0.164	5 230	0.14	1.96×10^{-5}	
Liquids	ρ	C_p	k	μ	σ
water	1000	4 190	0.60	1.00×10^{-3}	0.073
mercury	13 600	140	8.7	1.55×10^{-3}	0.51
ethanol	790	2 860	0.19	1.20×10^{-3}	0.022
R134a (25 °C)	1 210	1430	0.080	0.21×10^{-3}	
Solids	ρ	C_p	k	Notes	
mild steel	7 850	460	52		
stainless steel	7810	460	16	18% Ni & 8% Cr	
aluminium alloy	2720	880	170	Duralumin	
copper	8 950	380	400		
brass	8 410	380	120	30% Zn	
polyethylene	1 000	2 100	0.5	moderately high density	
expanded polystyrene	25		0.04	board	
concrete	2 400	900	1.0	moderately dense	
brick	1 800	750	0.6	common building brick	
wood	500	2 500	0.15	pine & dry	
glass	2 500	800	1.0	window	

^aNB. Constant C_p values in Table E.3 are averages over a range of temperature. $C_p(T)$ relationships used in Table E.5 are fits over a different temperature range. Neither will necessarily agree well with the 20 °C values tabulated here.

Psychrometric chart for moist air at atmospheric pressure

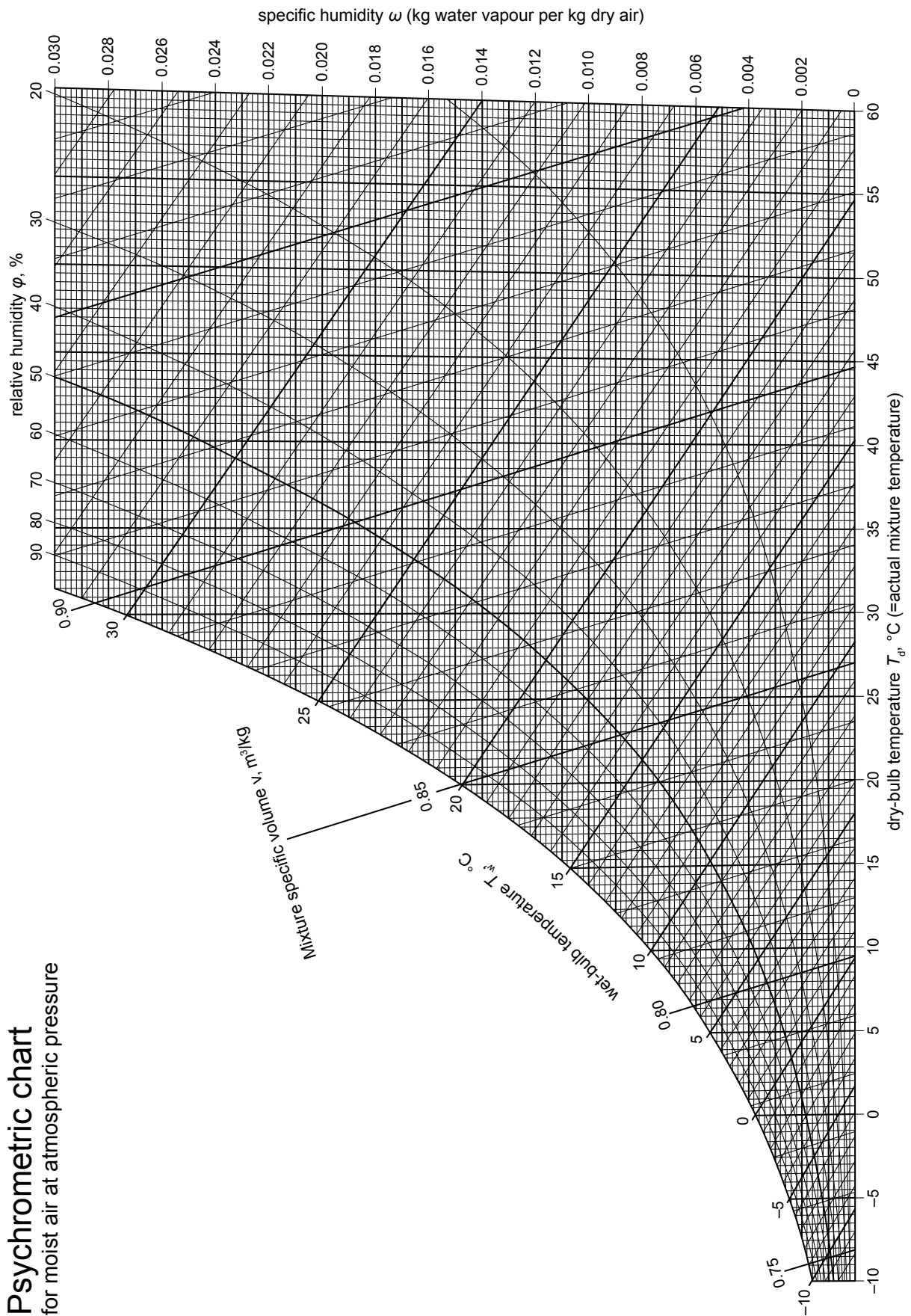


Figure E.2: Psychrometric Chart

E.12 Thermodynamic property tables for water/steam (IAPWS-IF97 formulation)

h	= specific enthalpy	kJ kg^{-1}
P	= absolute pressure	bar ($1 \text{ bar} = 10^5 \text{ Pa} = 10^5 \text{ N m}^{-2}$)
s	= specific entropy	$\text{kJ kg}^{-1} \text{ K}^{-1}$
T	= temperature	$^{\circ}\text{C}$
u	= specific internal energy	kJ kg^{-1}
v	= specific volume	$\text{m}^{-3} \text{ kg}^{-1}$

Subscripts:

f	= saturated liquid state
fg	= change between saturated liquid and saturated vapour states at constant pressure ($h_{fg} = h_g - h_f$)
g	= saturated vapour state
sat	= saturation state

Properties in these tables were evaluated from the Industrial Formulation 1997 of the International Association for the Properties of Water and Steam (IAPWS). There are small differences between these values and those in use in the Department of Mechanical Engineering up to 2003 (evaluated from the IAPWS 1984 Formulation for Scientific and General Use and 1986 Supplementary Release on Saturation Properties).

Triple point: $T = 0.01^{\circ}\text{C}$ $P = 0.006117 \text{ bar}$

Critical point: $T = 373.95^{\circ}\text{C}$ $P = 220.64 \text{ bar}$

u and s are chosen to be zero for saturated liquid at the triple point.

Linear interpolation in the tables is not advisable near the critical point.

Table E.19: Saturated water and steam — Temperature (triple point to 100 °C)

T °C	P bar (abs)	v_f m ³ kg ⁻¹	v_g m ³ kg ⁻¹	u_f kJ kg ⁻¹	u_g kJ kg ⁻¹	h_f kJ kg ⁻¹	h_{fg} kJ kg ⁻¹	h_g kJ kg ⁻¹	s_f kJ kg ⁻¹ K ⁻¹	s_g kJ kg ⁻¹ K ⁻¹
0.01	0.006117	0.001000	206.0	0	2374.9	0.000612	2500.9	2500.9	0	9.155
1	0.006571	0.001000	192.4	4.18	2376.3	4.177	2498.6	2502.7	0.0153	9.129
2	0.007060	0.001000	179.8	8.39	2377.7	8.392	2496.2	2504.6	0.0306	9.103
3	0.007581	0.001000	168.0	12.60	2379.0	12.60	2493.8	2506.4	0.0459	9.076
4	0.008135	0.001000	157.1	16.81	2380.4	16.81	2491.4	2508.2	0.0611	9.051
5	0.008726	0.001000	147.0	21.02	2381.8	21.02	2489.1	2510.1	0.0763	9.025
6	0.009354	0.001000	137.6	25.22	2383.2	25.22	2486.7	2511.9	0.0913	8.999
7	0.01002	0.001000	128.9	29.42	2384.5	29.42	2484.3	2513.7	0.1064	8.974
8	0.01073	0.001000	120.8	33.62	2385.9	33.63	2481.9	2515.6	0.1213	8.949
9	0.01148	0.001000	113.3	37.82	2387.3	37.82	2479.6	2517.4	0.1362	8.924
10	0.01228	0.001000	106.3	42.02	2388.7	42.02	2477.2	2519.2	0.1511	8.900
11	0.01313	0.001000	99.79	46.21	2390.0	46.22	2474.8	2521.1	0.1659	8.876
12	0.01403	0.001001	93.72	50.41	2391.4	50.41	2472.5	2522.9	0.1806	8.851
13	0.01498	0.001001	88.07	54.60	2392.8	54.60	2470.1	2524.7	0.1953	8.828
14	0.01599	0.001001	82.80	58.79	2394.1	58.79	2467.7	2526.5	0.2099	8.804
15	0.01706	0.001001	77.88	62.98	2395.5	62.98	2465.4	2528.4	0.2245	8.780
16	0.01819	0.001001	73.29	67.17	2396.9	67.17	2463.0	2530.2	0.2390	8.757
17	0.01938	0.001001	69.01	71.36	2398.3	71.36	2460.6	2532.0	0.2534	8.734
18	0.02065	0.001001	65.00	75.55	2399.6	75.55	2458.3	2533.8	0.2678	8.711
19	0.02198	0.001002	61.26	79.73	2401.0	79.73	2455.9	2535.7	0.2822	8.689
20	0.02339	0.001002	57.76	83.92	2402.4	83.92	2453.5	2537.5	0.2965	8.666
21	0.02488	0.001002	54.49	88.10	2403.7	88.10	2451.2	2539.3	0.3108	8.644
22	0.02645	0.001002	51.42	92.29	2405.1	92.29	2448.8	2541.1	0.3250	8.622
23	0.02811	0.001003	48.55	96.47	2406.4	96.47	2446.4	2542.9	0.3391	8.600
24	0.02986	0.001003	45.86	100.7	2407.8	100.7	2444.1	2544.7	0.3532	8.578
25	0.03170	0.001003	43.34	104.8	2409.2	104.8	2441.7	2546.5	0.3673	8.557
26	0.03364	0.001003	40.98	109.0	2410.5	109.0	2439.3	2548.4	0.3813	8.535
27	0.03568	0.001004	38.76	113.2	2411.9	113.2	2437.0	2550.2	0.3952	8.514
28	0.03783	0.001004	36.68	117.4	2413.2	117.4	2434.6	2552.0	0.4091	8.493
29	0.04009	0.001004	34.72	121.6	2414.6	121.6	2432.2	2553.8	0.4230	8.473
30	0.04247	0.001004	32.88	125.7	2415.9	125.7	2429.8	2555.6	0.4368	8.452
32	0.04759	0.001005	29.53	134.1	2418.7	134.1	2425.1	2559.2	0.4643	8.411
34	0.05325	0.001006	26.56	142.5	2421.4	142.5	2420.3	2562.8	0.4916	8.372
36	0.05948	0.001006	23.93	150.8	2424.0	150.8	2415.6	2566.4	0.5187	8.332
38	0.06632	0.001007	21.60	159.2	2426.7	159.2	2410.8	2570.0	0.5457	8.294
40	0.07384	0.001008	19.52	167.5	2429.4	167.5	2406.0	2573.5	0.5724	8.256
42	0.08209	0.001009	17.67	175.9	2432.1	175.9	2401.2	2577.1	0.5990	8.218
44	0.09112	0.001009	16.01	184.2	2434.8	184.3	2396.4	2580.7	0.6255	8.182
46	0.1010	0.001010	14.54	192.6	2437.4	192.6	2391.6	2584.2	0.6517	8.145
48	0.1118	0.001011	13.21	201.0	2440.1	201.0	2386.8	2587.8	0.6778	8.110
50	0.1235	0.001012	12.03	209.3	2442.8	209.3	2382.0	2591.3	0.7038	8.075
52	0.1363	0.001013	10.96	217.7	2445.4	217.7	2377.1	2594.8	0.7296	8.040
54	0.1502	0.001014	10.01	226.0	2448.0	226.1	2372.3	2598.4	0.7552	8.007
56	0.1653	0.001015	9.145	234.4	2450.7	234.4	2367.4	2601.9	0.7807	7.973
58	0.1817	0.001016	8.369	242.8	2453.3	242.8	2362.6	2605.4	0.8060	7.940
60	0.1995	0.001017	7.668	251.1	2455.9	251.2	2357.7	2608.8	0.8312	7.908
62	0.2187	0.001018	7.034	259.5	2458.5	259.5	2352.8	2612.3	0.8563	7.876
64	0.2394	0.001019	6.460	267.9	2461.1	267.9	2347.9	2615.8	0.8811	7.845
66	0.2618	0.001020	5.940	276.2	2463.7	276.3	2343.0	2619.2	0.9059	7.814
68	0.2860	0.001022	5.468	284.6	2466.3	284.6	2338.0	2622.7	0.9305	7.784
70	0.3120	0.001023	5.040	293.0	2468.9	293.0	2333.1	2626.1	0.9550	7.754
72	0.3400	0.001024	4.650	301.4	2471.4	301.4	2328.1	2629.5	0.9793	7.725
74	0.3701	0.001025	4.295	309.7	2474.0	309.8	2323.1	2632.9	1.004	7.696
76	0.4024	0.001026	3.971	318.1	2476.5	318.2	2318.1	2636.3	1.028	7.667
78	0.4370	0.001028	3.675	326.5	2479.0	326.6	2313.1	2639.7	1.052	7.639
80	0.4741	0.001029	3.405	334.9	2481.6	334.9	2308.1	2643.0	1.075	7.611
82	0.5139	0.001030	3.158	343.3	2484.1	343.3	2303.0	2646.4	1.099	7.584
84	0.5564	0.001032	2.932	351.7	2486.6	351.7	2297.9	2649.7	1.123	7.557
86	0.6017	0.001033	2.724	360.1	2489.0	360.1	2292.8	2653.0	1.146	7.530
88	0.6502	0.001035	2.534	368.5	2491.5	368.6	2287.7	2656.3	1.169	7.504
90	0.7018	0.001036	2.359	376.9	2494.0	377.0	2282.6	2659.5	1.193	7.478
92	0.7568	0.001037	2.198	385.3	2496.4	385.4	2277.4	2662.8	1.216	7.453
94	0.8154	0.001039	2.050	393.7	2498.8	393.8	2272.2	2666.0	1.239	7.427
96	0.8777	0.001040	1.914	402.1	2501.2	402.2	2267.0	2669.2	1.262	7.403
98	0.9439	0.001042	1.788	410.6	2503.6	410.7	2261.7	2672.4	1.284	7.378
100	1.0142	0.001043	1.672	419.0	2506.0	419.1	2256.5	2675.6	1.307	7.354

Table E.20: Saturated water and steam — Pressure (triple point to 2 bar)

P bar (abs)	T °C	v_f $\text{m}^3 \text{kg}^{-1}$	v_g $\text{m}^3 \text{kg}^{-1}$	u_f kJ kg^{-1}	u_g kJ kg^{-1}	h_f kJ kg^{-1}	h_{fg} kJ kg^{-1}	h_g kJ kg^{-1}	s_f $\text{kJ kg}^{-1} \text{K}^{-1}$	s_g $\text{kJ kg}^{-1} \text{K}^{-1}$
0.006117	0.01	0.001000	206.0	0	2374.9	0.000611783	2500.9	2500.9	0	9.155
0.008	3.76	0.001000	159.6	15.81	2380.1	15.809	2492.0	2507.8	0.0575	9.057
0.010	6.97	0.001000	129.2	29.30	2384.5	29.298	2484.4	2513.7	0.1059	8.975
0.012	9.65	0.001000	108.7	40.57	2388.2	40.569	2478.0	2518.6	0.1460	8.908
0.014	11.97	0.001001	93.90	50.28	2391.4	50.28	2472.5	2522.8	0.1802	8.852
0.016	14.01	0.001001	82.75	58.83	2394.2	58.84	2467.7	2526.6	0.2101	8.804
0.018	15.84	0.001001	74.01	66.49	2396.7	66.49	2463.4	2529.9	0.2366	8.761
0.020	17.50	0.001001	66.99	73.43	2398.9	73.43	2459.5	2532.9	0.2606	8.723
0.022	19.01	0.001002	61.21	79.79	2401.0	79.79	2455.9	2535.7	0.2824	8.688
0.024	20.41	0.001002	56.38	85.65	2402.9	85.66	2452.6	2538.2	0.3024	8.657
0.026	21.72	0.001002	52.27	91.11	2404.7	91.11	2449.5	2540.6	0.3210	8.628
0.028	22.94	0.001002	48.73	96.20	2406.4	96.20	2446.6	2542.8	0.3382	8.601
0.030	24.08	0.001003	45.66	100.99	2407.9	100.99	2443.9	2544.9	0.3543	8.577
0.035	26.67	0.001003	39.47	111.83	2411.4	111.84	2437.7	2549.6	0.3907	8.521
0.040	28.96	0.001004	34.79	121.40	2414.5	121.40	2432.3	2553.7	0.4224	8.473
0.045	31.01	0.001005	31.13	129.98	2417.3	129.98	2427.4	2557.4	0.4507	8.431
0.050	32.88	0.001005	28.19	137.76	2419.8	137.77	2423.0	2560.8	0.4763	8.394
0.060	36.16	0.001006	23.73	151.49	2424.3	151.49	2415.2	2566.7	0.5209	8.329
0.070	39.00	0.001007	20.53	163.36	2428.1	163.37	2408.4	2571.8	0.5591	8.275
0.080	41.51	0.001008	18.10	173.84	2431.4	173.85	2402.4	2576.2	0.5925	8.227
0.090	43.76	0.001009	16.20	183.25	2434.5	183.26	2397.0	2580.3	0.6223	8.186
0.100	45.81	0.001010	14.67	191.80	2437.2	191.81	2392.1	2583.9	0.6492	8.149
0.11	47.68	0.001011	13.41	199.65	2439.7	199.66	2387.6	2587.2	0.6737	8.115
0.12	49.42	0.001012	12.36	206.90	2442.0	206.91	2383.4	2590.3	0.6963	8.085
0.13	51.04	0.001013	11.46	213.65	2444.1	213.66	2379.5	2593.1	0.7172	8.057
0.14	52.55	0.001013	10.69	220.0	2446.1	220.0	2375.8	2595.8	0.7366	8.031
0.15	53.97	0.001014	10.02	225.9	2448.0	225.9	2372.4	2598.3	0.7548	8.007
0.16	55.31	0.001015	9.431	231.5	2449.8	231.6	2369.1	2600.7	0.7720	7.985
0.17	56.59	0.001015	8.909	236.9	2451.4	236.9	2366.0	2602.9	0.7882	7.964
0.18	57.80	0.001016	8.443	241.9	2453.0	241.9	2363.1	2605.0	0.8035	7.944
0.19	58.95	0.001017	8.025	246.8	2454.5	246.8	2360.2	2607.0	0.8181	7.925
0.20	60.06	0.001017	7.648	251.4	2456.0	251.4	2357.5	2608.9	0.8320	7.907
0.22	62.13	0.001018	6.994	260.1	2458.7	260.1	2352.5	2612.6	0.8579	7.874
0.24	64.05	0.001019	6.446	268.1	2461.2	268.1	2347.8	2615.9	0.8818	7.844
0.26	65.84	0.001020	5.979	275.6	2463.5	275.6	2343.4	2619.0	0.9040	7.817
0.28	67.52	0.001021	5.578	282.6	2465.7	282.6	2339.2	2621.8	0.9246	7.791
0.30	69.10	0.001022	5.229	289.2	2467.7	289.2	2335.3	2624.6	0.9439	7.767
0.35	72.68	0.001024	4.525	304.2	2472.3	304.3	2326.4	2630.7	0.9876	7.715
0.40	75.86	0.001026	3.993	317.5	2476.3	317.6	2318.5	2636.1	1.026	7.669
0.45	78.71	0.001028	3.576	329.5	2479.9	329.6	2311.3	2640.9	1.060	7.629
0.50	81.32	0.001030	3.240	340.4	2483.2	340.5	2304.7	2645.2	1.091	7.593
0.55	83.71	0.001032	2.964	350.5	2486.2	350.5	2298.7	2649.2	1.119	7.561
0.60	85.93	0.001033	2.732	359.8	2488.9	359.8	2293.0	2652.9	1.145	7.531
0.65	87.99	0.001035	2.535	368.5	2491.5	368.5	2287.7	2656.2	1.169	7.504
0.70	89.93	0.001036	2.365	376.6	2493.9	376.7	2282.7	2659.4	1.192	7.479
0.75	91.76	0.001037	2.217	384.3	2496.1	384.4	2278.0	2662.4	1.213	7.456
0.80	93.49	0.001038	2.087	391.6	2498.2	391.6	2273.5	2665.2	1.233	7.434
0.85	95.13	0.001040	1.972	398.5	2500.2	398.5	2269.3	2667.8	1.252	7.413
0.90	96.69	0.001041	1.869	405.0	2502.1	405.1	2265.2	2670.3	1.269	7.394
0.95	98.18	0.001042	1.777	411.3	2503.8	411.4	2261.3	2672.7	1.286	7.376
1.00	99.61	0.001043	1.694	417.3	2505.5	417.4	2257.5	2674.9	1.303	7.359
1.01325	99.97	0.001043	1.673	418.9	2506.0	419.0	2256.5	2675.5	1.307	7.354
1.1	102.3	0.001045	1.550	428.7	2508.7	428.8	2250.4	2679.2	1.333	7.327
1.2	104.8	0.001047	1.428	439.2	2511.6	439.3	2243.8	2683.1	1.361	7.298
1.3	107.1	0.001049	1.325	449.0	2514.3	449.1	2237.5	2686.6	1.387	7.271
1.4	109.3	0.001051	1.237	458.2	2516.9	458.4	2231.6	2690.0	1.411	7.246
1.5	111.4	0.001053	1.159	466.9	2519.2	467.1	2226.0	2693.1	1.434	7.223
1.6	113.3	0.001054	1.091	475.2	2521.4	475.3	2220.7	2696.0	1.455	7.201
1.7	115.1	0.001056	1.031	483.0	2523.5	483.2	2215.6	2698.8	1.475	7.181
1.8	116.9	0.001058	0.9775	490.5	2525.5	490.7	2210.7	2701.4	1.494	7.162
1.9	118.6	0.001059	0.9293	497.6	2527.3	497.8	2206.1	2703.9	1.513	7.144
2.0	120.2	0.001061	0.8857	504.5	2529.1	504.7	2201.6	2706.2	1.530	7.127

Table E.21: Saturated water and steam — Pressure (triple point to 2 bar)

P bar (abs)	T °C	v_f $\text{m}^3 \text{kg}^{-1}$	v_g $\text{m}^3 \text{kg}^{-1}$	u_f kJ kg^{-1}	u_g kJ kg^{-1}	h_f kJ kg^{-1}	h_{fg} kJ kg^{-1}	h_g kJ kg^{-1}	s_f $\text{kJ kg}^{-1} \text{K}^{-1}$	s_g $\text{kJ kg}^{-1} \text{K}^{-1}$
2.0	120.2	0.001061	0.8857	504.5	2529.1	504.7	2201.6	2706.2	1.530	7.127
2.2	123.3	0.001063	0.8101	517.4	2532.4	517.6	2193.0	2710.6	1.563	7.095
2.4	126.1	0.001066	0.7467	529.4	2535.4	529.6	2185.0	2714.6	1.593	7.066
2.6	128.7	0.001068	0.6928	540.6	2538.2	540.9	2177.4	2718.3	1.621	7.039
2.8	131.2	0.001071	0.6463	551.2	2540.8	551.5	2170.3	2721.7	1.647	7.015
3.0	133.5	0.001073	0.6058	561.1	2543.2	561.5	2163.4	2724.9	1.672	6.992
3.2	135.7	0.001075	0.5702	570.6	2545.4	570.9	2156.9	2727.9	1.695	6.970
3.4	137.8	0.001078	0.5387	579.6	2547.5	580.0	2150.7	2730.6	1.717	6.950
3.6	139.9	0.001080	0.5105	588.2	2549.5	588.6	2144.7	2733.3	1.738	6.931
3.8	141.8	0.001082	0.4852	596.4	2551.3	596.8	2138.9	2735.7	1.758	6.913
4.0	143.6	0.001084	0.4624	604.3	2553.1	604.7	2133.3	2738.1	1.777	6.895
4.2	145.4	0.001085	0.4417	611.9	2554.8	612.3	2127.9	2740.3	1.795	6.879
4.4	147.1	0.001087	0.4227	619.2	2556.4	619.7	2122.7	2742.4	1.812	6.863
4.6	148.7	0.001089	0.4054	626.2	2557.9	626.7	2117.6	2744.4	1.829	6.849
4.8	150.3	0.001091	0.3895	633.0	2559.3	633.6	2112.7	2746.3	1.845	6.834
5.0	151.8	0.001093	0.3748	639.6	2560.7	640.2	2107.9	2748.1	1.861	6.821
5.5	155.5	0.001097	0.3426	655.3	2563.9	655.9	2096.5	2752.3	1.897	6.789
6.0	158.8	0.001101	0.3156	669.8	2566.8	670.5	2085.6	2756.1	1.931	6.759
6.5	162.0	0.001104	0.2926	683.5	2569.4	684.2	2075.4	2759.6	1.963	6.732
7.0	165.0	0.001108	0.2728	696.4	2571.8	697.1	2065.6	2762.7	1.992	6.707
7.5	167.8	0.001111	0.2555	708.6	2574.0	709.4	2056.3	2765.6	2.020	6.684
8.0	170.4	0.001115	0.2403	720.1	2576.0	721.0	2047.3	2768.3	2.046	6.662
8.5	172.9	0.001118	0.2269	731.2	2577.9	732.1	2038.6	2770.8	2.071	6.641
9.0	175.4	0.001121	0.2149	741.7	2579.7	742.7	2030.3	2773.0	2.094	6.621
9.5	177.7	0.001124	0.2041	751.8	2581.3	752.9	2022.3	2775.2	2.117	6.603
10	179.9	0.001127	0.1943	761.6	2582.8	762.7	2014.4	2777.1	2.138	6.585
11	184.1	0.001133	0.1774	780.0	2585.5	781.2	1999.5	2780.7	2.179	6.552
12	188.0	0.001139	0.1632	797.1	2587.9	798.5	1985.3	2783.8	2.216	6.522
13	191.6	0.001144	0.1512	813.3	2590.0	814.8	1971.7	2786.5	2.251	6.494
14	195.0	0.001149	0.1408	828.5	2591.8	830.1	1958.8	2788.9	2.284	6.468
15	198.3	0.001154	0.1317	843.0	2593.5	844.7	1946.3	2791.0	2.315	6.443
16	201.4	0.001159	0.1237	856.8	2594.9	858.6	1934.3	2792.9	2.344	6.420
17	204.3	0.001163	0.1167	869.9	2596.2	871.9	1922.6	2794.5	2.371	6.398
18	207.1	0.001168	0.1104	882.5	2597.3	884.6	1911.4	2796.0	2.398	6.378
19	209.8	0.001172	0.1047	894.6	2598.3	896.8	1900.4	2797.3	2.423	6.358
20	212.4	0.001177	0.09958	906.3	2599.2	908.6	1889.8	2798.4	2.447	6.339
21	214.9	0.001181	0.09493	917.5	2600.0	920.0	1879.4	2799.4	2.470	6.321
22	217.3	0.001185	0.09070	928.4	2600.7	931.0	1869.2	2800.2	2.492	6.304
23	219.6	0.001189	0.08681	938.9	2601.3	941.6	1859.3	2800.9	2.514	6.287
24	221.8	0.001193	0.08324	949.1	2601.8	952.0	1849.6	2801.5	2.534	6.271
25	224.0	0.001197	0.07995	959.0	2602.2	962.0	1840.1	2802.0	2.554	6.256
26	226.1	0.001201	0.07690	968.6	2602.5	971.7	1830.7	2802.5	2.574	6.241
27	228.1	0.001205	0.07407	978.0	2602.8	981.2	1821.5	2802.8	2.593	6.227
28	230.1	0.001209	0.07143	987.1	2603.0	990.5	1812.5	2803.0	2.611	6.213
29	232.0	0.001213	0.06897	996.0	2603.2	999.5	1803.6	2803.2	2.628	6.199
30	233.9	0.001217	0.06666	1004.7	2603.3	1008.4	1794.9	2803.3	2.646	6.186
31	235.7	0.001220	0.06450	1013.2	2603.3	1017.0	1786.3	2803.3	2.662	6.173
32	237.5	0.001224	0.06247	1021.5	2603.3	1025.5	1777.8	2803.2	2.679	6.160
33	239.2	0.001228	0.06056	1029.7	2603.3	1033.7	1769.4	2803.1	2.695	6.148
34	240.9	0.001231	0.05876	1037.6	2603.2	1041.8	1761.1	2803.0	2.710	6.136
35	242.6	0.001235	0.05706	1045.5	2603.0	1049.8	1753.0	2802.7	2.725	6.125
36	244.2	0.001239	0.05545	1053.1	2602.9	1057.6	1744.9	2802.5	2.740	6.113
37	245.8	0.001242	0.05392	1060.6	2602.6	1065.2	1736.9	2802.1	2.755	6.102
38	247.3	0.001246	0.05247	1068.0	2602.4	1072.8	1729.0	2801.8	2.769	6.091
39	248.9	0.001249	0.05109	1075.3	2602.1	1080.2	1721.2	2801.4	2.783	6.080
40	250.4	0.001253	0.04978	1082.4	2601.8	1087.4	1713.5	2800.9	2.797	6.070
41	251.8	0.001256	0.04853	1089.4	2601.4	1094.6	1705.8	2800.4	2.810	6.059
42	253.3	0.001259	0.04733	1096.3	2601.1	1101.6	1698.2	2799.9	2.823	6.049
43	254.7	0.001263	0.04619	1103.1	2600.6	1108.6	1690.7	2799.3	2.836	6.039
44	256.1	0.001266	0.04510	1109.8	2600.2	1115.4	1683.2	2798.7	2.849	6.029
45	257.4	0.001270	0.04406	1116.4	2599.7	1122.1	1675.9	2798.0	2.861	6.020

Table E.22: Saturated water and steam — Pressure (triple point to 2 bar)

P bar (abs)	T °C	v_f $\text{m}^3 \text{kg}^{-1}$	v_g $\text{m}^3 \text{kg}^{-1}$	u_f kJ kg^{-1}	u_g kJ kg^{-1}	h_f kJ kg^{-1}	h_{fg} kJ kg^{-1}	h_g kJ kg^{-1}	s_f $\text{kJ kg}^{-1} \text{K}^{-1}$	s_g $\text{kJ kg}^{-1} \text{K}^{-1}$
45	257.4	0.001270	0.04406	1116.4	2599.7	1122.1	1675.9	2798.0	2.861	6.020
46	258.8	0.001273	0.04306	1122.9	2599.2	1128.8	1668.5	2797.3	2.874	6.010
47	260.1	0.001276	0.04210	1129.3	2598.7	1135.3	1661.2	2796.6	2.886	6.001
48	261.4	0.001280	0.04118	1135.7	2598.2	1141.8	1654.0	2795.8	2.898	5.992
49	262.7	0.001283	0.04030	1141.9	2597.6	1148.2	1646.8	2795.0	2.909	5.983
50	263.9	0.001286	0.03945	1148.1	2597.0	1154.5	1639.7	2794.2	2.921	5.974
51	265.2	0.001290	0.03863	1154.2	2596.4	1160.7	1632.7	2793.4	2.932	5.965
52	266.4	0.001293	0.03784	1160.2	2595.7	1166.9	1625.6	2792.5	2.943	5.956
53	267.6	0.001296	0.03708	1166.1	2595.1	1173.0	1618.6	2791.6	2.954	5.948
54	268.8	0.001300	0.03635	1172.0	2594.4	1179.0	1611.7	2790.7	2.965	5.939
55	270.0	0.001303	0.03564	1177.8	2593.7	1184.9	1604.8	2789.7	2.976	5.931
56	271.1	0.001306	0.03496	1183.5	2593.0	1190.8	1597.9	2788.7	2.986	5.922
57	272.3	0.001309	0.03430	1189.2	2592.2	1196.6	1591.1	2787.7	2.997	5.914
58	273.4	0.001313	0.03366	1194.8	2591.5	1202.4	1584.3	2786.7	3.007	5.906
59	274.5	0.001316	0.03305	1200.3	2590.7	1208.1	1577.6	2785.6	3.017	5.898
60	275.6	0.001319	0.03245	1205.8	2589.9	1213.7	1570.8	2784.6	3.027	5.890
62	277.7	0.001326	0.03131	1216.6	2588.2	1224.9	1557.5	2782.3	3.047	5.874
64	279.8	0.001332	0.03024	1227.3	2586.5	1235.8	1544.2	2780.0	3.067	5.859
66	281.9	0.001339	0.02923	1237.7	2584.7	1246.5	1531.1	2777.6	3.085	5.844
68	283.9	0.001345	0.02828	1247.9	2582.8	1257.1	1518.1	2775.1	3.104	5.829
70	285.8	0.001352	0.02738	1258.0	2580.9	1267.4	1505.1	2772.6	3.122	5.815
72	287.7	0.001358	0.02653	1267.9	2578.9	1277.7	1492.3	2769.9	3.140	5.800
74	289.6	0.001365	0.02572	1277.6	2576.9	1287.7	1479.5	2767.2	3.157	5.786
76	291.4	0.001371	0.02495	1287.2	2574.8	1297.6	1466.8	2764.4	3.174	5.772
78	293.2	0.001378	0.02422	1296.7	2572.6	1307.4	1454.1	2761.5	3.191	5.758
80	295.0	0.001385	0.02353	1306.0	2570.4	1317.1	1441.5	2758.6	3.208	5.745
82	296.7	0.001391	0.02286	1315.2	2568.1	1326.6	1429.0	2755.6	3.224	5.731
84	298.4	0.001398	0.02223	1324.3	2565.8	1336.0	1416.5	2752.5	3.240	5.718
86	300.1	0.001405	0.02163	1333.3	2563.4	1345.3	1404.0	2749.4	3.256	5.705
88	301.7	0.001411	0.02105	1342.1	2560.9	1354.5	1391.6	2746.2	3.271	5.692
90	303.3	0.001418	0.02049	1350.9	2558.4	1363.7	1379.2	2742.9	3.287	5.679
92	304.9	0.001425	0.01996	1359.6	2555.9	1372.7	1366.9	2739.5	3.302	5.666
94	306.5	0.001432	0.01945	1368.1	2553.3	1381.6	1354.5	2736.1	3.317	5.653
96	308.0	0.001439	0.01896	1376.6	2550.6	1390.4	1342.2	2732.6	3.331	5.641
98	309.5	0.001446	0.01849	1385.0	2547.9	1399.2	1329.9	2729.1	3.346	5.628
100	311.0	0.001453	0.01803	1393.3	2545.1	1407.9	1317.6	2725.5	3.360	5.616
105	314.6	0.001470	0.01697	1413.8	2538.0	1429.3	1286.9	2716.1	3.396	5.585
110	318.1	0.001489	0.01599	1433.9	2530.5	1450.3	1256.1	2706.4	3.430	5.555
115	321.4	0.001507	0.01510	1453.6	2522.6	1470.9	1225.3	2696.2	3.464	5.524
120	324.7	0.001526	0.01427	1473.0	2514.4	1491.3	1194.3	2685.6	3.496	5.494
125	327.8	0.001546	0.01350	1492.1	2505.7	1511.5	1163.0	2674.5	3.529	5.464
130	330.9	0.001566	0.01279	1511.0	2496.7	1531.4	1131.5	2662.9	3.561	5.434
135	333.8	0.001588	0.01212	1529.8	2487.2	1551.2	1099.6	2650.8	3.592	5.404
140	336.7	0.001610	0.01149	1548.3	2477.2	1570.9	1067.2	2638.1	3.623	5.373
145	339.5	0.001633	0.01090	1566.8	2466.8	1590.5	1034.3	2624.8	3.654	5.342
150	342.2	0.001657	0.01034	1585.3	2455.8	1610.2	1000.7	2610.9	3.684	5.311
155	344.8	0.001682	0.009811	1603.8	2444.1	1629.9	966.4	2596.2	3.715	5.279
160	347.4	0.001710	0.009308	1622.3	2431.9	1649.7	931.1	2580.8	3.746	5.246
165	349.9	0.001738	0.008828	1641.0	2418.9	1669.7	894.9	2564.6	3.776	5.213
170	352.3	0.001769	0.008369	1660.0	2405.1	1690.0	857.4	2547.4	3.808	5.179
175	354.7	0.001803	0.007927	1679.2	2390.4	1710.8	818.4	2529.1	3.839	5.143
180	357.0	0.001839	0.007499	1698.9	2374.6	1732.0	777.5	2509.5	3.872	5.106
185	359.3	0.001880	0.007082	1719.2	2357.4	1754.0	734.4	2488.4	3.905	5.066
190	361.5	0.001925	0.006673	1740.3	2338.6	1776.9	688.5	2465.4	3.940	5.025
195	363.6	0.001977	0.006267	1762.5	2317.8	1801.1	638.9	2440.0	3.976	4.980
200	365.7	0.002039	0.005858	1786.3	2294.2	1827.1	584.3	2411.4	4.015	4.930
205	367.8	0.002114	0.005438	1812.6	2266.7	1855.9	522.3	2378.2	4.059	4.874
210	369.8	0.002212	0.004988	1842.9	2232.8	1889.4	448.1	2337.5	4.109	4.806
215	371.8	0.002360	0.004463	1882.1	2186.2	1932.8	349.4	2282.2	4.175	4.717
220	373.7	0.002750	0.003577	1961.4	2085.5	2021.9	142.3	2164.2	4.311	4.531
220.64	373.95	0.003106	0.003106	2019.0	2019.0	2087.5	0	2087.5	4.412	4.412

Table E.23: Subcooled water and Superheated Steam (triple point to 0.1 bar)

T(°C)	0.006117 bar ($T_{\text{sat}} = 0.01^\circ\text{C}$)				0.01 bar ($T_{\text{sat}} = 7.0^\circ\text{C}$)				0.05 bar ($T_{\text{sat}} = 32.9^\circ\text{C}$)				0.1 bar ($T_{\text{sat}} = 45.8^\circ\text{C}$)				T(°C)
	v	u	h	s	v	u	h	s	v	u	h	s	v	u	h	s	
0.01	206.0	2374.9	2500.9	9.155	0.001000	0.000007	0.001007	0.0000	0.001000	0.000081	0.005082	0.0000	0.001000	0.000174	0.01018	0.000001	0.01
20	221.1	2403.1	2538.4	9.288	135.2	2403.0	2538.2	9.060	0.001002	83.92	2574.4	8.438	0.001002	83.92	83.93	0.2965	20
40	236.2	2431.3	2575.8	9.411	144.5	2431.2	2575.7	9.184	28.85	2430.1	2612.3	8.555	0.001008	167.5	167.5	0.5724	40
60	251.3	2459.5	2613.3	9.527	153.7	2459.5	2613.2	9.300	30.71	2458.7	2650.8	8.666	15.34	2457.8	2611.2	8.233	60
80	266.4	2487.9	2650.8	9.637	163.0	2487.8	2650.8	9.410	32.57	2487.3	2687.0	8.770	16.27	2486.7	2649.3	8.344	80
100	281.5	2516.4	2688.6	9.741	172.2	2516.3	2688.5	9.514	34.42	2516.0	2688.0	8.770	17.20	2515.5	2687.4	8.449	100
120	296.6	2545.0	2726.5	9.840	181.4	2545.0	2726.4	9.613	36.27	2544.7	2726.1	8.869	18.12	2544.3	2725.6	8.548	120
140	311.7	2573.9	2764.6	9.934	190.7	2573.9	2764.5	9.707	38.12	2573.6	2764.2	8.964	19.05	2573.3	2763.8	8.643	140
160	326.8	2602.9	2802.8	10.02	199.9	2602.9	2802.8	9.798	39.97	2602.7	2802.6	9.055	19.98	2602.5	2802.2	8.734	160
180	341.9	2632.2	2841.3	10.11	209.1	2632.2	2841.3	9.885	41.82	2632.0	2841.1	9.141	20.90	2631.8	2840.8	8.821	180
200	357.0	2661.6	2880.0	10.20	218.4	2661.6	2880.0	9.968	43.66	2661.5	2879.8	9.225	21.83	2661.3	2879.6	8.905	200
220	372.1	2691.3	2918.9	10.28	227.6	2691.3	2918.9	10.05	45.51	2691.2	2918.8	9.306	22.75	2691.1	2918.6	8.986	220
240	387.2	2721.3	2958.1	10.35	236.8	2721.2	2958.1	10.13	47.36	2721.1	2957.9	9.384	23.67	2721.0	2957.8	9.063	240
260	402.3	2751.4	2997.5	10.43	246.1	2751.4	2997.5	10.20	49.20	2751.3	2997.3	9.459	24.60	2751.2	2997.2	9.139	260
280	417.4	2781.8	3037.1	10.50	255.3	2781.8	3037.1	10.27	51.05	2781.7	3037.0	9.532	25.52	2781.6	3036.8	9.212	280
300	432.5	2812.4	3077.0	10.57	264.5	2812.4	3077.0	10.35	52.90	2812.4	3076.9	9.603	26.45	2812.3	3076.7	9.283	300
320	447.6	2843.3	3117.1	10.64	273.7	2843.3	3117.1	10.41	54.75	2843.3	3117.0	9.672	27.37	2843.2	3116.9	9.351	320
340	462.6	2874.5	3157.4	10.71	283.0	2874.5	3157.4	10.48	56.59	2874.4	3157.4	9.738	28.29	2874.3	3157.3	9.418	340
360	477.7	2905.9	3198.1	10.77	292.2	2905.8	3198.1	10.55	58.44	2905.8	3198.0	9.804	29.22	2905.7	3197.9	9.484	360
380	492.8	2937.5	3238.9	10.84	301.4	2937.5	3238.9	10.61	60.28	2937.4	3238.9	9.867	30.14	2937.4	3238.8	9.547	380
400	507.9	2969.4	3280.1	10.90	310.7	2969.4	3280.1	10.67	62.13	2969.4	3280.0	9.929	31.06	2969.3	3279.9	9.609	400
420	523.0	3001.6	3321.5	10.96	319.9	3001.6	3321.5	10.73	63.98	3001.5	3321.4	9.990	31.99	3001.5	3321.3	9.670	420
440	538.1	3034.0	3363.2	11.02	329.1	3034.0	3363.1	10.79	65.82	3034.0	3363.1	10.05	32.91	3033.9	3363.0	9.729	440
460	553.2	3066.7	3405.1	11.08	338.4	3066.7	3405.1	10.85	67.67	3066.7	3405.0	10.11	33.83	3066.6	3405.0	9.787	460
480	568.3	3099.7	3447.3	11.13	347.6	3099.7	3447.3	10.91	69.52	3099.7	3447.2	10.16	34.76	3099.6	3447.2	9.844	480
500	583.4	3132.9	3489.8	11.19	356.8	3132.9	3489.8	10.96	71.36	3132.9	3489.7	10.22	35.68	3132.9	3489.7	9.900	500
520	598.5	3166.5	3532.5	11.24	366.1	3166.5	3532.5	11.02	73.21	3166.4	3532.5	10.27	36.60	3166.4	3532.4	9.954	520
540	613.6	3200.3	3575.6	11.30	375.3	3200.3	3575.6	11.07	75.06	3200.2	3575.5	10.33	37.53	3200.2	3575.5	10.01	540
560	628.7	3234.4	3618.9	11.35	384.5	3234.4	3618.9	11.12	76.90	3234.3	3618.8	10.38	38.45	3234.3	3618.8	10.06	560
580	643.7	3268.7	3662.5	11.40	393.7	3268.7	3662.5	11.18	78.75	3268.7	3662.4	10.43	39.37	3268.7	3662.4	10.11	580
600	658.8	3303.4	3706.3	11.45	403.0	3303.4	3706.3	11.23	80.59	3303.3	3706.3	10.48	40.30	3303.3	3706.3	10.16	600
640	689.0	3373.5	3794.9	11.55	421.4	3373.5	3794.9	11.33	84.29	3373.5	3794.9	10.58	42.14	3373.4	3794.9	10.26	640
680	719.2	3444.8	3884.7	11.65	439.9	3444.8	3884.7	11.42	87.98	3444.7	3884.6	10.68	43.99	3444.7	3884.6	10.36	680
720	749.4	3517.2	3975.5	11.74	458.4	3517.2	3975.5	11.51	91.67	3517.2	3975.5	10.77	45.84	3517.1	3975.5	10.45	720
760	779.6	3590.7	4067.5	11.83	476.8	3590.7	4067.5	11.61	95.36	3590.7	4067.5	10.86	47.68	3590.7	4067.5	10.54	760
800	809.7	3665.4	4160.7	11.92	495.3	3665.4	4160.7	11.69	99.06	3665.4	4160.6	10.95	49.53	3665.3	4160.6	10.63	800

Table E.24: Subcooled water and Superheated Steam (0.1 bar to 1 atmosphere)

T(°C)	0.2 bar ($T_{\text{sat}} = 60.1\text{ }^{\circ}\text{C}$)				0.5 bar ($T_{\text{sat}} = 81.3\text{ }^{\circ}\text{C}$)				1 bar ($T_{\text{sat}} = 99.6\text{ }^{\circ}\text{C}$)				1.01325 bar ($T_{\text{sat}} = 100.0\text{ }^{\circ}\text{C}$)				T(°C)
	v	u	h	s	v	u	h	s	v	u	h	s	v	u	h	s	
0.01	0.001000	0.000360	0.02036	0.00000	0.001000	0.000915	0.05092	0.00000	0.001000	0.001841	0.1019	0.00001	0.001000	0.001865	0.1032	0.00001	0.01
20	0.001002	83.92	83.94	0.296	0.001002	83.91	83.96	0.2965	0.001002	83.91	84.01	0.2965	0.001002	83.91	84.01	0.2965	20
40	0.001008	167.5	167.6	0.572	0.001008	167.5	167.6	0.5724	0.001008	167.5	167.6	0.5724	0.001008	167.5	167.6	0.5724	40
60	0.001017	251.1	251.2	0.831	0.001017	251.1	251.2	0.8312	0.001017	251.1	251.2	0.8312	0.001017	251.1	251.2	0.8312	60
80	8.118	2485.3	2647.7	8.020	0.001029	334.9	335.0	1.075	0.001029	334.9	335.0	1.075	0.001029	334.9	335.0	1.075	80
100	8.586	2514.5	2686.2	8.126	3.419	2511.5	2682.4	7.695	1.696	2506.2	2675.8	7.361	1.673	2506.0	2675.6	7.355	100
120	9.052	2543.6	2724.6	8.227	3.608	2541.3	2721.7	7.798	1.793	2537.3	2716.6	7.468	1.770	2537.2	2716.5	7.461	120
140	9.517	2572.7	2763.1	8.322	3.796	2570.9	2760.7	7.895	1.889	2567.8	2756.7	7.567	1.864	2567.7	2756.6	7.561	140
160	9.98	2602.0	2801.6	8.413	3.983	2600.5	2799.7	7.987	1.984	2598.0	2796.4	7.661	1.958	2597.9	2796.3	7.655	160
180	10.44	2631.4	2840.3	8.500	4.170	2630.2	2838.7	8.075	2.079	2628.1	2836.0	7.750	2.051	2628.1	2835.9	7.744	180
200	10.91	2661.0	2879.1	8.584	4.356	2660.0	2877.8	8.159	2.172	2658.2	2875.5	7.836	2.144	2658.2	2875.4	7.829	200
220	11.37	2690.8	2918.2	8.665	4.542	2689.9	2917.0	8.240	2.266	2688.4	2915.0	7.917	2.236	2688.4	2915.0	7.911	220
240	11.83	2720.8	2957.4	8.743	4.728	2720.3	2956.4	8.319	2.360	2718.7	2954.7	7.996	2.329	2718.7	2954.6	7.990	240
260	12.30	2751.0	2996.9	8.818	4.913	2750.3	2996.0	8.394	2.453	2749.2	2994.4	8.072	2.421	2749.1	2994.4	8.066	260
280	12.76	2781.4	3036.6	8.892	5.099	2780.8	3035.8	8.468	2.546	2779.8	3034.4	8.146	2.512	2779.8	3034.4	8.140	280
300	13.22	2812.1	3076.5	8.962	5.284	2811.6	3075.8	8.539	2.639	2810.7	3074.5	8.217	2.604	2810.6	3074.5	8.211	300
320	13.68	2843.0	3116.7	9.031	5.469	2842.5	3116.0	8.608	2.732	2841.7	3114.9	8.286	2.696	2841.7	3114.9	8.280	320
340	14.14	2874.2	3157.1	9.098	5.654	2873.7	3156.5	8.675	2.825	2873.0	3155.5	8.354	2.788	2873.0	3155.4	8.347	340
360	14.61	2905.6	3197.7	9.164	5.840	2905.2	3197.2	8.740	2.917	2904.5	3196.2	8.419	2.879	2904.5	3196.2	8.413	360
380	15.07	2937.3	3238.6	9.227	6.025	2936.9	3238.1	8.804	3.010	2936.3	3237.3	8.483	2.971	2936.2	3237.2	8.477	380
400	15.53	2969.2	3279.8	9.289	6.209	2968.8	3279.3	8.866	3.103	2968.3	3278.5	8.545	3.062	2968.3	3278.5	8.539	400
420	15.99	3001.4	3321.2	9.350	6.394	3001.1	3320.8	8.927	3.195	3000.5	3320.1	8.606	3.154	3000.5	3320.0	8.600	420
440	16.45	3033.8	3362.9	9.409	6.579	3033.5	3362.5	8.986	3.288	3033.0	3361.8	8.665	3.245	3033.0	3361.8	8.659	440
460	16.92	3066.5	3404.8	9.467	6.764	3066.3	3404.5	9.044	3.381	3065.8	3403.9	8.723	3.336	3065.8	3403.8	8.717	460
480	17.38	3099.5	3447.1	9.524	6.949	3099.3	3446.7	9.101	3.473	3098.8	3446.2	8.780	3.428	3098.8	3446.1	8.774	480
500	17.84	3132.8	3489.6	9.580	7.134	3132.6	3489.2	9.156	3.566	3132.2	3488.7	8.836	3.519	3132.1	3488.7	8.830	500
520	18.30	3166.3	3532.3	9.634	7.319	3166.1	3532.0	9.211	3.658	3165.7	3531.5	8.891	3.610	3165.7	3531.5	8.885	520
540	18.76	3200.1	3575.4	9.688	7.503	3199.9	3575.1	9.265	3.751	3199.6	3574.6	8.944	3.701	3199.6	3574.6	8.938	540
560	19.22	3234.2	3618.7	9.741	7.688	3234.0	3618.4	9.317	3.843	3233.7	3618.0	8.997	3.793	3233.7	3618.0	8.991	560
580	19.69	3268.6	3662.3	9.792	7.873	3268.4	3662.1	9.369	3.936	3268.1	3661.6	9.049	3.884	3268.1	3661.6	9.043	580
600	20.15	3303.2	3706.2	9.843	8.058	3303.1	3706.0	9.420	4.028	3302.8	3705.6	9.100	3.975	3302.8	3705.6	9.094	600
640	21.07	3373.4	3794.8	9.942	8.427	3373.2	3794.6	9.519	4.213	3373.0	3794.3	9.199	4.158	3373.0	3794.2	9.193	640
680	21.99	3444.7	3884.6	10.04	8.797	3444.5	3884.4	9.615	4.398	3444.3	3884.1	9.295	4.340	3444.3	3884.1	9.289	680
720	22.92	3517.1	3975.4	10.13	9.166	3517.0	3975.3	9.709	4.582	3516.7	3975.0	9.389	4.522	3516.7	3975.0	9.383	720
760	23.84	3590.6	4067.4	10.22	9.535	3590.5	4067.3	9.800	4.767	3590.3	4067.0	9.480	4.705	3590.3	4067.0	9.474	760
800	24.76	3665.3	4160.6	10.31	9.905	3665.2	4160.4	9.888	4.952	3665.0	4160.2	9.568	4.887	3665.0	4160.2	9.562	800

Table E.25: Subcooled water and Superheated Steam (2 bar to 8 bar)

T(°C)	2 bar ($T_{\text{sat}} = 120.2\text{ }^{\circ}\text{C}$)				4 bar ($T_{\text{sat}} = 143.6\text{ }^{\circ}\text{C}$)				6 bar ($T_{\text{sat}} = 158.8\text{ }^{\circ}\text{C}$)				8 bar ($T_{\text{sat}} = 170.4\text{ }^{\circ}\text{C}$)				T(°C)
	v	u	h	s	v	u	h	s	v	u	h	s	v	u	h	s	
0.01	0.001000	0.003688	0.2037	0.00001	0.001000	0.007365	0.4074	0.00003	0.001000	0.0110	0.0110	0.00004	0.001000	0.0147	0.8145	0.00005	0.01
20	0.001002	83.91	84.11	0.2965	0.001002	83.89	84.29	0.2964	0.001002	83.88	84.48	0.2964	0.001001	83.87	84.67	0.2963	20
40	0.001008	167.5	167.7	0.5724	0.001008	167.5	167.9	0.5723	0.001008	167.5	168.1	0.5722	0.001008	167.4	168.2	0.5721	40
60	0.001017	251.1	251.3	0.8311	0.001017	251.1	251.5	0.8310	0.001017	251.0	251.6	0.8309	0.001017	251.0	251.8	0.8308	60
80	0.001029	334.9	335.1	1.075	0.001029	334.8	335.2	1.075	0.001029	334.8	335.4	1.075	0.001029	334.7	335.5	1.075	80
100	0.001043	419.0	419.2	1.307	0.001043	418.9	419.3	1.307	0.001043	418.8	419.5	1.307	0.001043	418.8	419.6	1.306	100
120	0.001060	503.6	503.8	1.528	0.001060	503.5	503.9	1.528	0.001060	503.4	504.1	1.527	0.001060	503.4	504.2	1.527	120
140	0.001080	588.8	589.2	1.739	0.001080	588.8	589.2	1.739	0.001080	588.7	589.4	1.739	0.001079	588.6	589.5	1.739	140
160	0.001102	674.8	675.7	1.943	0.001102	674.8	675.7	1.943	0.001102	674.8	675.7	1.943	0.001102	674.8	675.7	1.943	160
180	0.001128	761.1	761.9	2.158	0.001128	761.1	761.9	2.158	0.001128	761.1	761.9	2.158	0.001128	761.1	761.9	2.158	180
200	0.001158	848.8	849.8	2.374	0.001158	848.8	849.8	2.374	0.001158	848.8	849.8	2.374	0.001158	848.8	849.8	2.374	200
220	0.001192	937.9	939.1	2.591	0.001192	937.9	939.1	2.591	0.001192	937.9	939.1	2.591	0.001192	937.9	939.1	2.591	220
240	0.001230	1029.1	1031.4	2.808	0.001230	1029.1	1031.4	2.808	0.001230	1029.1	1031.4	2.808	0.001230	1029.1	1031.4	2.808	240
260	0.001272	1123.4	1126.8	3.025	0.001272	1123.4	1126.8	3.025	0.001272	1123.4	1126.8	3.025	0.001272	1123.4	1126.8	3.025	260
280	0.001318	1220.8	1225.2	3.242	0.001318	1220.8	1225.2	3.242	0.001318	1220.8	1225.2	3.242	0.001318	1220.8	1225.2	3.242	280
300	0.001368	1321.2	1326.6	3.459	0.001368	1321.2	1326.6	3.459	0.001368	1321.2	1326.6	3.459	0.001368	1321.2	1326.6	3.459	300
320	0.001422	1424.6	1431.0	3.676	0.001422	1424.6	1431.0	3.676	0.001422	1424.6	1431.0	3.676	0.001422	1424.6	1431.0	3.676	320
340	0.001480	1531.0	1538.4	3.893	0.001480	1531.0	1538.4	3.893	0.001480	1531.0	1538.4	3.893	0.001480	1531.0	1538.4	3.893	340
360	0.001542	1640.4	1648.8	4.110	0.001542	1640.4	1648.8	4.110	0.001542	1640.4	1648.8	4.110	0.001542	1640.4	1648.8	4.110	360
380	0.001608	1752.8	1762.2	4.327	0.001608	1752.8	1762.2	4.327	0.001608	1752.8	1762.2	4.327	0.001608	1752.8	1762.2	4.327	380
400	0.001678	1868.2	1879.6	4.544	0.001678	1868.2	1879.6	4.544	0.001678	1868.2	1879.6	4.544	0.001678	1868.2	1879.6	4.544	400
420	0.001752	1986.6	1999.0	4.761	0.001752	1986.6	1999.0	4.761	0.001752	1986.6	1999.0	4.761	0.001752	1986.6	1999.0	4.761	420
440	0.001830	2108.0	2122.4	4.978	0.001830	2108.0	2122.4	4.978	0.001830	2108.0	2122.4	4.978	0.001830	2108.0	2122.4	4.978	440
460	0.001912	2232.4	2248.8	5.195	0.001912	2232.4	2248.8	5.195	0.001912	2232.4	2248.8	5.195	0.001912	2232.4	2248.8	5.195	460
480	0.002000	2359.8	2378.2	5.412	0.002000	2359.8	2378.2	5.412	0.002000	2359.8	2378.2	5.412	0.002000	2359.8	2378.2	5.412	480
500	0.002102	2489.2	2510.6	5.629	0.002102	2489.2	2510.6	5.629	0.002102	2489.2	2510.6	5.629	0.002102	2489.2	2510.6	5.629	500
520	0.002218	2621.6	2645.0	5.846	0.002218	2621.6	2645.0	5.846	0.002218	2621.6	2645.0	5.846	0.002218	2621.6	2645.0	5.846	520
540	0.002348	2757.0	2783.4	6.063	0.002348	2757.0	2783.4	6.063	0.002348	2757.0	2783.4	6.063	0.002348	2757.0	2783.4	6.063	540
560	0.002492	2895.4	2924.8	6.280	0.002492	2895.4	2924.8	6.280	0.002492	2895.4	2924.8	6.280	0.002492	2895.4	2924.8	6.280	560
580	0.002650	3036.8	3069.2	6.497	0.002650	3036.8	3069.2	6.497	0.002650	3036.8	3069.2	6.497	0.002650	3036.8	3069.2	6.497	580
600	0.002822	3181.2	3217.6	6.714	0.002822	3181.2	3217.6	6.714	0.002822	3181.2	3217.6	6.714	0.002822	3181.2	3217.6	6.714	600
640	0.003218	3521.6	3570.0	7.141	0.003218	3521.6	3570.0	7.141	0.003218	3521.6	3570.0	7.141	0.003218	3521.6	3570.0	7.141	640
680	0.003652	3862.0	3923.4	7.568	0.003652	3862.0	3923.4	7.568	0.003652	3862.0	3923.4	7.568	0.003652	3862.0	3923.4	7.568	680
720	0.004136	4202.4	4277.8	7.995	0.004136	4202.4	4277.8	7.995	0.004136	4202.4	4277.8	7.995	0.004136	4202.4	4277.8	7.995	720
760	0.004680	4542.8	4624.2	8.422	0.004680	4542.8	4624.2	8.422	0.004680	4542.8	4624.2	8.422	0.004680	4542.8	4624.2	8.422	760
800	0.005282	4883.2	4975.6	8.849	0.005282	4883.2	4975.6	8.849	0.005282	4883.2	4975.6	8.849	0.005282	4883.2	4975.6	8.849	800

Table E.26: Subcooled water and Superheated Steam (10 bar to 40 bar)

T(°C)	10 bar ($T_{\text{sat}} = 179.9\text{ }^{\circ}\text{C}$)				20 bar ($T_{\text{sat}} = 212.4\text{ }^{\circ}\text{C}$)				30 bar ($T_{\text{sat}} = 233.9\text{ }^{\circ}\text{C}$)				40 bar ($T_{\text{sat}} = 250.4\text{ }^{\circ}\text{C}$)				T(°C)
	v	u	h	s	v	u	h	s	v	u	h	s	v	u	h	s	
0.01	0.001000	0.01827	1.018	0.00007	0.000999	0.03601	2.034	0.00013	0.000999	0.05321	3.049	0.00019	0.000998	0.06989	4.063	0.00024	0.01
20	0.001001	83.86	84.86	0.2963	0.001001	83.80	85.80	0.2961	0.001000	83.74	86.74	0.2959	0.001000	83.68	87.68	0.2957	20
40	0.001007	167.4	168.4	0.5720	0.001007	167.3	169.3	0.5717	0.001007	167.2	170.2	0.5713	0.001006	167.1	171.1	0.5709	40
60	0.001017	251.0	252.0	0.8307	0.001016	250.8	252.8	0.8302	0.001016	250.6	253.7	0.8296	0.001015	250.4	254.5	0.8291	60
80	0.001029	334.7	335.7	1.075	0.001028	334.4	336.5	1.074	0.001028	334.2	337.3	1.073	0.001027	334.0	338.1	1.073	80
100	0.001043	418.7	419.8	1.306	0.001042	418.4	420.5	1.306	0.001042	418.2	421.3	1.305	0.001041	417.9	422.0	1.304	100
120	0.001060	503.3	504.3	1.527	0.001059	502.9	505.1	1.526	0.001059	502.6	505.8	1.525	0.001058	502.2	506.5	1.524	120
140	0.001079	588.5	589.6	1.739	0.001079	588.1	590.3	1.738	0.001078	587.7	590.9	1.737	0.001077	587.3	591.6	1.736	140
160	0.001102	674.7	675.8	1.942	0.001101	674.2	676.4	1.941	0.001100	673.7	677.0	1.940	0.001100	673.2	677.6	1.939	160
180	0.001144	777.4	778.5	2.138	0.001127	761.4	763.7	2.138	0.001126	760.8	764.2	2.137	0.001125	760.2	764.7	2.135	180
200	0.001194	883.0	884.1	2.330	0.001156	850.3	852.6	2.330	0.001155	849.5	853.0	2.329	0.001154	848.8	853.4	2.327	200
220	0.001270	998.6	999.7	2.517	0.001222	940.3	943.8	2.517	0.001189	940.3	943.8	2.517	0.001188	939.3	944.1	2.515	220
240	0.001344	1124.1	1125.2	2.699	0.001289	1026.8	1030.3	2.699	0.001228	1026.8	1030.3	2.699	0.001228	1026.8	1030.3	2.699	240
260	0.001420	1260.7	1261.8	2.877	0.001366	1138.5	1142.0	2.877	0.001311	1138.5	1142.0	2.877	0.001311	1138.5	1142.0	2.877	260
280	0.001500	1408.5	1409.6	3.051	0.001454	1266.2	1269.7	3.051	0.001400	1266.2	1269.7	3.051	0.001400	1266.2	1269.7	3.051	280
300	0.001584	1567.6	1568.7	3.221	0.001544	1407.1	1410.6	3.221	0.001488	1407.1	1410.6	3.221	0.001488	1407.1	1410.6	3.221	300
320	0.001672	1738.1	1739.2	3.387	0.001639	1561.6	1565.1	3.387	0.001582	1561.6	1565.1	3.387	0.001582	1561.6	1565.1	3.387	320
340	0.001764	1920.2	1921.3	3.549	0.001720	1730.1	1733.6	3.549	0.001672	1730.1	1733.6	3.549	0.001672	1730.1	1733.6	3.549	340
360	0.001860	2114.9	2116.0	3.707	0.001816	1914.6	1918.1	3.707	0.001764	1914.6	1918.1	3.707	0.001764	1914.6	1918.1	3.707	360
380	0.001960	2322.2	2323.3	3.861	0.001920	2114.9	2118.4	3.861	0.001860	2114.9	2118.4	3.861	0.001860	2114.9	2118.4	3.861	380
400	0.002064	2542.1	2543.2	4.011	0.002020	2322.2	2325.7	4.011	0.001960	2322.2	2325.7	4.011	0.001960	2322.2	2325.7	4.011	400
420	0.002172	2774.6	2775.7	4.157	0.002124	2542.1	2545.6	4.157	0.002064	2542.1	2545.6	4.157	0.002064	2542.1	2545.6	4.157	420
440	0.002284	3019.7	3020.8	4.300	0.002234	2774.6	2778.1	4.300	0.002172	2774.6	2778.1	4.300	0.002172	2774.6	2778.1	4.300	440
460	0.002399	3277.4	3278.5	4.439	0.002346	3019.7	3023.2	4.439	0.002284	3019.7	3023.2	4.439	0.002284	3019.7	3023.2	4.439	460
480	0.002517	3547.7	3548.8	4.574	0.002461	3277.4	3280.9	4.574	0.002399	3277.4	3280.9	4.574	0.002399	3277.4	3280.9	4.574	480
500	0.002638	3830.7	3831.8	4.706	0.002580	3547.7	3551.2	4.706	0.002517	3547.7	3551.2	4.706	0.002517	3547.7	3551.2	4.706	500
520	0.002762	4126.4	4127.5	4.835	0.002704	3830.7	3834.2	4.835	0.002638	3830.7	3834.2	4.835	0.002638	3830.7	3834.2	4.835	520
540	0.002889	4434.9	4436.0	4.961	0.002828	4126.4	4129.9	4.961	0.002762	4126.4	4129.9	4.961	0.002762	4126.4	4129.9	4.961	540
560	0.003019	4756.4	4757.5	5.084	0.002954	4434.9	4438.4	5.084	0.002889	4434.9	4438.4	5.084	0.002889	4434.9	4438.4	5.084	560
580	0.003152	5091.1	5092.2	5.205	0.003083	4756.4	4759.9	5.205	0.003019	4756.4	4759.9	5.205	0.003019	4756.4	4759.9	5.205	580
600	0.003288	5439.1	5440.2	5.324	0.003214	5091.1	5094.6	5.324	0.003152	5091.1	5094.6	5.324	0.003152	5091.1	5094.6	5.324	600
640	0.003541	6124.9	6126.0	5.502	0.003467	5830.7	5834.2	5.502	0.003393	5830.7	5834.2	5.502	0.003393	5830.7	5834.2	5.502	640
680	0.003800	6861.8	6862.9	5.699	0.003724	6617.6	6621.1	5.699	0.003650	6617.6	6621.1	5.699	0.003650	6617.6	6621.1	5.699	680
720	0.004064	7660.7	7661.8	5.906	0.003980	7469.1	7472.6	5.906	0.003906	7469.1	7472.6	5.906	0.003906	7469.1	7472.6	5.906	720
760	0.004333	8522.2	8523.3	6.121	0.004244	8384.6	8388.1	6.121	0.004170	8384.6	8388.1	6.121	0.004170	8384.6	8388.1	6.121	760
800	0.004607	9456.4	9457.5	6.344	0.004508	9372.8	9376.3	6.344	0.004434	9372.8	9376.3	6.344	0.004434	9372.8	9376.3	6.344	800

Table E.27: Subcooled water and Superheated Steam (50 bar to 80 bar)

T(°C)	50 bar ($T_{\text{sat}} = 263.9\text{ }^{\circ}\text{C}$)				60 bar ($T_{\text{sat}} = 275.6\text{ }^{\circ}\text{C}$)				70 bar ($T_{\text{sat}} = 285.8\text{ }^{\circ}\text{C}$)				80 bar ($T_{\text{sat}} = 295.0\text{ }^{\circ}\text{C}$)				T(°C)
	v	u	h	s	v	u	h	s	v	u	h	s	v	u	h	s	
0.01	0.000998	0.08604	5.074	0.00029	0.000997	0.10167	6.085	0.00034	0.000997	0.11679	7.094	0.00038	0.000996	0.13139	8.101	0.00042	0.01
20	0.001000	83.62	88.61	0.2955	0.000999	83.55	89.55	0.2952	0.000999	83.49	90.48	0.2950	0.000998	83.43	91.42	0.2948	20
40	0.001006	166.9	172.0	0.5705	0.001005	166.8	172.8	0.5701	0.001005	166.7	173.7	0.5697	0.001004	166.6	174.6	0.5693	40
60	0.001015	250.3	255.3	0.8286	0.001014	250.1	256.2	0.8280	0.001014	249.9	257.0	0.8275	0.001014	249.7	257.8	0.8270	60
80	0.001027	333.8	338.9	1.072	0.001026	333.5	339.7	1.071	0.001026	333.3	340.5	1.071	0.001025	333.1	341.3	1.070	80
100	0.001041	417.6	422.8	1.303	0.001040	417.3	423.5	1.302	0.001040	417.0	424.3	1.302	0.001039	416.7	425.0	1.301	100
120	0.001058	501.9	507.2	1.523	0.001057	501.5	507.9	1.523	0.001057	501.2	508.6	1.522	0.001056	500.8	509.3	1.521	120
140	0.001077	586.8	592.2	1.734	0.001076	586.4	592.9	1.733	0.001076	586.0	593.5	1.732	0.001075	585.6	594.2	1.731	140
160	0.001099	672.7	678.1	1.938	0.001098	672.1	678.7	1.936	0.001097	671.6	679.3	1.935	0.001097	671.1	679.9	1.934	160
180	0.001124	759.6	765.2	2.134	0.001123	759.0	765.7	2.133	0.001122	758.4	766.2	2.131	0.001122	757.8	766.8	2.130	180
200	0.001153	848.0	853.8	2.325	0.001152	847.3	854.2	2.324	0.001151	846.6	854.6	2.322	0.001150	845.9	855.1	2.321	200
220	0.001187	938.4	944.4	2.513	0.001186	937.6	944.7	2.511	0.001184	936.7	945.0	2.509	0.001183	935.8	945.3	2.507	220
240	0.001227	1031.5	1037.7	2.698	0.001225	1030.4	1037.8	2.696	0.001224	1029.3	1037.9	2.694	0.001222	1028.3	1038.0	2.692	240
260	0.001275	1128.4	1134.8	2.884	0.001273	1127.0	1134.6	2.881	0.001271	1125.6	1134.5	2.879	0.001269	1124.2	1134.3	2.876	260
280	0.04227	2646.7	2658.1	6.091	0.03320	2606.0	2805.2	5.928	0.001331	1227.0	1236.3	3.066	0.001328	1225.2	1235.8	3.063	280
300	0.04535	2698.9	2925.6	6.211	0.03619	2668.3	2885.5	6.070	0.02949	2633.4	2839.8	5.934	0.02428	2592.1	2786.4	5.794	300
320	0.04813	2745.5	2986.2	6.315	0.03878	2720.9	2953.5	6.187	0.03201	2693.8	2917.9	6.067	0.02684	2663.6	2878.4	5.951	320
340	0.05073	2786.7	3042.4	6.408	0.04114	2768.1	3014.9	6.289	0.03423	2745.9	2965.5	6.180	0.02899	2721.9	2953.9	6.077	340
360	0.05319	2829.7	3095.6	6.493	0.04334	2811.9	3072.0	6.380	0.03626	2793.2	3047.0	6.278	0.03092	2773.3	3020.6	6.184	360
380	0.05555	2869.1	3146.8	6.573	0.04542	2853.6	3126.1	6.465	0.03816	2837.3	3104.4	6.368	0.03268	2820.3	3081.8	6.279	380
400	0.05784	2907.4	3196.6	6.648	0.04742	2893.6	3178.2	6.543	0.03996	2879.4	3159.1	6.450	0.03435	2864.5	3139.3	6.366	400
420	0.06007	2945.0	3245.3	6.719	0.04936	2932.6	3228.8	6.617	0.04169	2919.9	3211.8	6.527	0.03593	2906.8	3194.2	6.446	420
440	0.06225	2982.0	3293.3	6.788	0.05124	2970.9	3278.3	6.688	0.04337	2959.4	3263.0	6.600	0.03745	2947.6	3247.3	6.522	440
460	0.06439	3018.7	3340.7	6.853	0.05308	3008.5	3327.0	6.755	0.04500	2998.1	3313.1	6.669	0.03893	2987.5	3298.9	6.593	460
480	0.06650	3055.2	3387.7	6.917	0.05489	3045.9	3375.2	6.820	0.04659	3036.3	3362.5	6.736	0.04036	3026.6	3349.5	6.661	480
500	0.06858	3091.6	3434.5	6.978	0.05667	3082.9	3422.9	6.882	0.04816	3074.1	3411.3	6.800	0.04177	3065.2	3399.4	6.726	500
520	0.07064	3127.8	3481.1	7.037	0.05843	3119.8	3470.4	6.943	0.04970	3111.7	3459.6	6.861	0.04315	3103.5	3448.6	6.789	520
540	0.07268	3164.1	3527.5	7.095	0.06016	3156.7	3517.6	7.002	0.05121	3149.1	3507.6	6.921	0.04450	3141.5	3497.5	6.850	540
560	0.07470	3200.4	3574.0	7.152	0.06188	3193.5	3564.7	7.059	0.05271	3186.4	3555.4	6.979	0.04584	3179.3	3546.0	6.909	560
580	0.07671	3236.8	3620.4	7.207	0.06358	3230.3	3611.8	7.115	0.05420	3223.7	3603.1	7.036	0.04716	3217.0	3594.3	6.966	580
600	0.07870	3273.3	3666.8	7.260	0.06526	3267.2	3658.8	7.169	0.05566	3261.0	3650.6	7.091	0.04846	3254.7	3642.4	7.022	600
640	0.08265	3346.7	3759.9	7.365	0.06860	3341.2	3752.8	7.275	0.05857	3335.7	3745.6	7.197	0.05104	3330.1	3738.4	7.130	640
680	0.08657	3420.6	3853.5	7.465	0.07190	3415.7	3847.1	7.376	0.06143	3410.8	3840.8	7.299	0.05357	3405.8	3834.4	7.232	680
720	0.09045	3495.3	3947.6	7.562	0.07517	3490.9	3941.9	7.473	0.06426	3486.4	3936.2	7.397	0.05607	3481.9	3930.5	7.331	720
760	0.09431	3570.8	4042.4	7.655	0.07842	3566.8	4037.3	7.567	0.06706	3562.7	4032.2	7.492	0.05855	3558.6	4027.0	7.427	760
800	0.09815	3647.1	4137.9	7.746	0.08164	3643.4	4133.3	7.658	0.06985	3639.7	4128.7	7.584	0.06101	3636.0	4124.0	7.519	800

Table E.28: Subcooled water and Superheated Steam (90 bar to 140 bar)

T(°C)	90 bar ($T_{\text{sat}} = 303.3^{\circ}\text{C}$)				100 bar ($T_{\text{sat}} = 311.0^{\circ}\text{C}$)				120 bar ($T_{\text{sat}} = 324.7^{\circ}\text{C}$)				140 bar ($T_{\text{sat}} = 336.7^{\circ}\text{C}$)				T(°C)
	v	u	h	s	v	u	h	s	v	u	h	s	v	u	h	s	
0.01	0.000996	0.1455	9.107	0.00046	0.000995	0.1591	10.11	0.00049	0.000994	0.1847	12.12	0.00055	0.000993	0.2084	14.11	0.00059	0.01
20	0.000998	83.37	92.35	0.2946	0.000997	83.31	93.29	0.2944	0.000996	83.19	95.15	0.2939	0.000996	83.07	97.01	0.2935	20
40	0.001004	166.5	175.5	0.5689	0.001003	166.3	176.4	0.5685	0.001003	166.1	178.1	0.5678	0.001002	165.9	179.9	0.5670	40
60	0.001013	249.6	258.7	0.8265	0.001013	249.4	259.5	0.8259	0.001012	249.1	261.2	0.8249	0.001011	248.7	262.9	0.8238	60
80	0.001025	332.9	342.1	1.070	0.001024	332.6	342.9	1.069	0.001023	332.2	344.5	1.068	0.001023	331.7	346.1	1.066	80
100	0.001039	416.4	425.8	1.300	0.001038	416.2	426.5	1.299	0.001038	415.6	428.1	1.298	0.001037	415.1	429.6	1.296	100
120	0.001055	500.5	510.0	1.520	0.001055	500.2	510.7	1.519	0.001054	499.5	512.1	1.517	0.001053	498.8	513.5	1.516	120
140	0.001074	585.2	594.8	1.730	0.001074	584.8	595.5	1.729	0.001073	583.9	596.8	1.727	0.001071	583.1	598.1	1.725	140
160	0.001096	670.7	680.5	1.933	0.001095	670.2	681.1	1.932	0.001094	669.2	682.3	1.929	0.001093	668.2	683.5	1.927	160
180	0.001121	757.2	767.3	2.129	0.001120	756.6	767.8	2.127	0.001118	755.4	768.9	2.125	0.001117	754.3	769.9	2.122	180
200	0.001149	845.1	855.5	2.319	0.001148	844.4	855.9	2.318	0.001146	843.0	856.8	2.315	0.001144	841.6	857.7	2.312	200
220	0.001182	934.9	945.6	2.506	0.001181	934.1	945.9	2.504	0.001179	932.4	946.5	2.500	0.001176	930.7	947.2	2.497	220
240	0.001221	1027.2	1038.2	2.690	0.001219	1026.1	1038.3	2.688	0.001216	1024.0	1038.6	2.683	0.001213	1022.0	1039.0	2.679	240
260	0.001267	1122.8	1134.2	2.873	0.001265	1121.5	1134.1	2.871	0.001262	1118.8	1134.0	2.866	0.001258	1116.3	1133.9	2.861	260
280	0.001325	1223.4	1235.3	3.059	0.001323	1221.6	1234.8	3.056	0.001317	1218.1	1233.9	3.050	0.001312	1214.8	1233.1	3.044	280
300	0.001402	1331.6	1344.3	3.253	0.001398	1329.1	1343.1	3.248	0.001390	1324.3	1340.9	3.240	0.001382	1319.6	1339.0	3.231	300
320	0.02271	2629.5	2833.9	5.835	0.01927	2589.9	2782.7	5.713	0.001494	1442.4	1480.3	3.444	0.001480	1435.2	1455.9	3.432	320
340	0.02486	2895.8	2919.6	5.977	0.02149	2667.2	2882.1	5.878	0.01621	2596.9	2793.5	5.672	0.01200	2504.4	2672.4	5.429	340
360	0.02672	2752.0	2992.5	6.094	0.02333	2729.3	2962.6	6.007	0.01812	2678.4	2895.9	5.837	0.01423	2617.2	2816.4	5.661	360
380	0.02840	2802.4	3058.0	6.196	0.02495	2783.6	3033.1	6.117	0.01971	2742.6	2979.1	5.966	0.01587	2696.1	2918.3	5.819	380
400	0.02996	2849.1	3118.8	6.287	0.02644	2833.0	3097.4	6.214	0.02111	2798.6	3051.9	6.076	0.01724	2760.9	3002.2	5.946	400
420	0.03144	2893.2	3176.1	6.371	0.02783	2879.2	3157.5	6.302	0.02239	2849.6	3118.2	6.173	0.01846	2817.7	3076.1	6.054	420
440	0.03284	2935.5	3231.1	6.450	0.02915	2923.1	3214.6	6.383	0.02358	2897.1	3180.1	6.261	0.01958	2869.5	3143.6	6.150	440
460	0.03420	2976.6	3284.4	6.523	0.03041	2965.4	3269.5	6.459	0.02471	2942.3	3238.8	6.343	0.02062	2918.0	3206.7	6.237	460
480	0.03551	3016.7	3336.3	6.593	0.03163	3006.6	3322.9	6.531	0.02579	2985.8	3295.2	6.418	0.02160	2964.1	3266.5	6.318	480
500	0.03690	3056.2	3387.3	6.660	0.03281	3046.9	3375.1	6.599	0.02683	3028.8	3350.0	6.490	0.02255	3008.4	3324.1	6.393	500
520	0.03805	3095.1	3437.6	6.724	0.03397	3086.6	3426.3	6.665	0.02784	3069.3	3403.4	6.558	0.02345	3051.5	3379.8	6.464	520
540	0.03928	3133.7	3487.2	6.786	0.03510	3125.9	3476.9	6.728	0.02882	3109.9	3455.8	6.624	0.02433	3093.5	3434.2	6.532	540
560	0.04049	3172.1	3536.5	6.846	0.03621	3164.8	3526.9	6.789	0.02978	3150.0	3507.4	6.696	0.02519	3134.9	3487.5	6.597	560
580	0.04168	3210.3	3585.4	6.904	0.03730	3203.5	3576.5	6.847	0.03072	3189.8	3558.4	6.747	0.02602	3175.7	3540.1	6.659	580
600	0.04286	3248.4	3634.2	6.960	0.03838	3242.1	3625.8	6.905	0.03165	3229.2	3609.0	6.806	0.02684	3216.1	3591.9	6.719	600
640	0.04518	3324.6	3731.2	7.069	0.04049	3319.0	3723.9	7.014	0.03346	3307.6	3709.2	6.918	0.02844	3296.1	3694.3	6.834	640
680	0.04746	3400.8	3828.0	7.173	0.04257	3395.8	3821.5	7.119	0.03523	3385.7	3808.5	7.024	0.03000	3375.5	3795.4	6.942	680
720	0.04971	3477.4	3924.8	7.272	0.04461	3472.9	3919.0	7.219	0.03697	3463.8	3907.5	7.126	0.03151	3454.6	3895.8	7.045	720
760	0.05193	3554.5	4021.9	7.368	0.04663	3550.4	4016.7	7.316	0.03868	3542.2	4006.4	7.223	0.03301	3533.9	3995.9	7.144	760
800	0.05413	3632.2	4119.4	7.461	0.04862	3628.5	4114.7	7.409	0.04037	3621.0	4105.4	7.318	0.03448	3613.4	4096.0	7.239	800

Table E.29: Subcooled water and Superheated Steam (160 bar to 220 bar)

T(°C)	160 bar ($T_{\text{sat}} = 347.4\text{ °C}$)					180 bar ($T_{\text{sat}} = 357.0\text{ °C}$)					200 bar ($T_{\text{sat}} = 365.7\text{ °C}$)					220 bar ($T_{\text{sat}} = 373.7\text{ °C}$)					T(°C)
	v	u	h	s		v	u	h	s		v	u	h	s		v	u	h	s		
0.01	0.000992	0.2302	16.11	0.00061		0.000991	0.2501	18.09	0.00063		0.000990	0.2680	20.08	0.00062		0.000989	0.2842	22.05	0.00061		0.01
20	0.000995	82.95	98.87	0.2930		0.000994	82.83	100.7	0.2926		0.000993	82.71	102.6	0.2921		0.000992	82.59	104.4	0.2916		20
40	0.001001	165.6	181.7	0.5662		0.001000	165.4	183.4	0.5654		0.000999	165.2	185.2	0.5646		0.000998	165.0	186.9	0.5639		40
60	0.001010	248.4	264.5	0.8228		0.001009	248.1	266.2	0.8218		0.001008	247.7	267.9	0.8207		0.001008	247.4	269.6	0.8197		60
80	0.001022	331.3	347.6	1.065		0.001021	330.9	349.2	1.064		0.001020	330.4	350.8	1.062		0.001019	330.0	352.4	1.061		80
100	0.001036	414.5	431.1	1.295		0.001035	414.0	432.6	1.293		0.001034	413.4	434.1	1.292		0.001033	412.9	435.6	1.290		100
120	0.001052	498.1	515.0	1.514		0.001051	497.5	516.4	1.512		0.001050	496.8	517.8	1.510		0.001049	496.2	519.2	1.509		120
140	0.001070	582.3	599.5	1.723		0.001069	581.5	600.8	1.721		0.001068	580.7	602.1	1.719		0.001067	580.0	603.4	1.718		140
160	0.001091	667.3	684.7	1.925		0.001090	666.3	685.9	1.923		0.001089	665.4	687.2	1.920		0.001087	664.5	688.4	1.918		160
180	0.001115	753.2	771.0	2.120		0.001114	752.0	772.1	2.117		0.001112	750.9	773.2	2.115		0.001111	749.8	774.2	2.112		180
200	0.001143	840.3	858.6	2.309		0.001141	838.9	859.5	2.306		0.001139	837.6	860.4	2.303		0.001137	836.3	861.3	2.300		200
220	0.001174	929.0	947.8	2.494		0.001172	927.4	948.5	2.490		0.001170	925.8	949.2	2.487		0.001168	924.3	949.9	2.484		220
240	0.001211	1019.9	1039.3	2.675		0.001208	1018.0	1039.7	2.671		0.001205	1016.0	1040.1	2.668		0.001203	1014.1	1040.6	2.664		240
260	0.001254	1113.7	1133.8	2.856		0.001251	1111.3	1133.8	2.851		0.001247	1108.9	1133.8	2.847		0.001244	1106.5	1133.9	2.842		260
280	0.001307	1211.5	1232.5	3.038		0.001302	1208.4	1231.8	3.032		0.001298	1205.3	1231.3	3.026		0.001293	1202.4	1230.8	3.021		280
300	0.001375	1315.2	1337.2	3.224		0.001368	1311.0	1335.6	3.216		0.001361	1306.9	1334.1	3.209		0.001355	1303.0	1332.8	3.202		300
320	0.001467	1428.5	1451.9	3.420		0.001456	1422.2	1448.4	3.409		0.001445	1416.4	1445.3	3.399		0.001435	1410.9	1442.5	3.390		320
340	0.001616	1561.4	1587.3	3.645		0.001591	1550.1	1578.7	3.625		0.001569	1540.1	1571.5	3.608		0.001551	1531.2	1565.3	3.593		340
360	0.01106	2538.7	2715.6	5.462		0.004624	2145.8	2233.9	4.658		0.002365	1834.4	1876.1	4.101		0.002047	1768.2	1803.9	3.987		360
380	0.01288	2642.2	2848.3	5.668		0.01042	2577.4	2764.9	5.505		0.008258	2494.0	2659.2	5.314		0.004125	2183.2	2279.4	4.700		380
400	0.01428	2719.0	2947.5	5.818		0.01191	2671.8	2886.3	5.688		0.009950	2617.8	2816.8	5.552		0.008255	2554.2	2735.8	5.405		400
420	0.01548	2783.2	3030.9	5.940		0.01312	2745.7	2981.9	5.828		0.01120	2704.5	2928.5	5.716		0.009588	2659.0	2869.9	5.602		420
440	0.01655	2840.2	3105.0	6.045		0.01417	2808.9	3064.0	5.945		0.01225	2775.3	3020.3	5.847		0.01085	2739.3	2973.6	5.749		440
460	0.01753	2892.5	3173.0	6.139		0.01512	2865.6	3137.7	6.047		0.01317	2837.2	3100.6	5.958		0.01156	2807.2	3061.6	5.871		460
480	0.01845	2941.5	3236.7	6.225		0.01599	2917.9	3205.7	6.138		0.01401	2893.2	3173.4	6.056		0.01238	2867.5	3139.9	5.976		480
500	0.01932	2988.1	3297.3	6.305		0.01681	2967.1	3269.7	6.222		0.01479	2945.3	3241.2	6.145		0.01314	2922.8	3211.8	6.070		500
520	0.02016	3033.1	3355.6	6.379		0.01759	3014.1	3330.7	6.300		0.01553	2994.6	3305.2	6.226		0.01384	2974.5	3279.0	6.156		520
540	0.02096	3076.7	3412.1	6.449		0.01833	3059.5	3389.5	6.373		0.01623	3041.8	3366.4	6.303		0.01451	3023.7	3342.9	6.236		540
560	0.02174	3119.4	3467.3	6.516		0.01905	3103.6	3446.6	6.443		0.01690	3087.5	3425.6	6.374		0.01514	3071.0	3404.1	6.310		560
580	0.02250	3161.4	3521.4	6.581		0.01975	3146.8	3502.4	6.509		0.01755	3132.0	3483.0	6.443		0.01575	3116.8	3463.4	6.381		580
600	0.02324	3202.8	3574.6	6.642		0.02043	3189.3	3557.0	6.572		0.01818	3175.5	3539.2	6.508		0.01635	3161.6	3521.2	6.448		600
640	0.02467	3284.5	3679.2	6.759		0.02174	3272.7	3664.0	6.692		0.01940	3260.7	3648.7	6.630		0.01748	3248.6	3633.2	6.573		640
680	0.02607	3365.2	3782.2	6.870		0.02301	3354.7	3768.9	6.804		0.02056	3344.2	3755.5	6.745		0.01856	3333.5	3742.0	6.690		680
720	0.02742	3445.4	3884.1	6.975		0.02424	3436.0	3872.3	6.911		0.02169	3426.6	3860.5	6.853		0.01961	3417.2	3848.6	6.799		720
760	0.02875	3525.5	3985.5	7.075		0.02544	3517.1	3975.0	7.012		0.02279	3508.6	3964.4	6.955		0.02063	3500.1	3953.8	6.903		760
800	0.03006	3605.7	4086.6	7.171		0.02662	3598.1	4077.2	7.109		0.02387	3590.4	4067.7	7.053		0.02162	3582.6	4058.2	7.002		800

Table E.30: Supercritical steam (250 bar to 500 bar)

$T(^{\circ}\text{C})$	250 bar				300 bar				400 bar				500 bar				$T(^{\circ}\text{C})$
	v	u	h	s	v	u	h	s	v	u	h	s	v	u	h	s	
0.01	0.000988	0.3049	25	0.00056	0.000986	0.3308	29.9	0.00043	0.000981	0.3511	39.6	-0.00008	0.000977	0.3323	49.17	-0.00087	0.01
20	0.000991	82.41	107.18	0.2909	0.000989	82.12	111.8	0.2897	0.000985	81.52	120.9	0.2872	0.00098	80.93	130	0.2845	20
40	0.000997	164.6	189.5	0.5627	0.000995	164.1	193.9	0.5607	0.000991	163	202.6	0.5568	0.000987	161.9	211.3	0.5528	40
60	0.001006	246.9	272.1	0.8181	0.001004	246.1	276.2	0.8156	0.001	244.6	284.6	0.8105	0.000996	243.1	292.9	0.8054	60
80	0.001018	329.4	354.8	1.059	0.001016	328.3	358.8	1.056	0.001011	326.3	366.8	1.05	0.001007	324.4	374.7	1.044	80
100	0.001031	412.1	437.9	1.288	0.001029	410.8	441.7	1.284	0.001024	408.3	449.3	1.277	0.00102	405.9	456.9	1.27	100
120	0.001047	495.2	521.4	1.506	0.001045	493.6	525	1.502	0.00104	490.6	532.2	1.494	0.001035	487.7	539.4	1.486	120
140	0.001065	578.8	605.4	1.715	0.001062	576.9	608.8	1.71	0.001057	573.3	615.6	1.701	0.001052	569.8	622.4	1.692	140
160	0.001085	663.1	690.2	1.915	0.001082	660.8	693.3	1.91	0.001076	656.5	699.6	1.899	0.00107	652.4	706	1.889	160
180	0.001108	748.2	775.9	2.108	0.001105	745.5	778.7	2.102	0.001098	740.5	784.4	2.091	0.001091	735.6	790.2	2.079	180
200	0.001135	834.4	862.7	2.296	0.00113	831.2	865.1	2.289	0.001122	825.2	870.1	2.276	0.001115	819.6	875.3	2.263	200
220	0.001164	921.9	951.1	2.479	0.001159	918.2	953	2.471	0.00115	911.1	957.1	2.456	0.001141	904.4	961.5	2.441	220
240	0.001199	1011.3	1041.3	2.658	0.001193	1006.8	1042.6	2.649	0.001181	998.4	1045.6	2.632	0.001171	990.5	1049	2.615	240
260	0.001239	1103.1	1134.1	2.835	0.001231	1097.6	1134.6	2.825	0.001217	1087.4	1136.1	2.805	0.001204	1078.1	1138.3	2.786	260
280	0.001287	1198.1	1230.2	3.012	0.001277	1191.3	1229.6	3	0.001259	1178.8	1229.1	2.976	0.001243	1167.5	1229.7	2.954	280
300	0.001346	1297.4	1331.1	3.192	0.001332	1288.7	1328.7	3.176	0.001308	1273.1	1325.4	3.147	0.001288	1259.3	1323.7	3.121	300
320	0.001421	1403.2	1438.7	3.376	0.001401	1391.5	1433.5	3.355	0.001368	1371.3	1426	3.319	0.001341	1354.2	1421.2	3.289	320
340	0.001526	1519.3	1557.5	3.573	0.001493	1502.3	1547.1	3.544	0.001443	1474.8	1532.5	3.496	0.001405	1452.8	1523.1	3.457	340
360	0.001858	1714.6	1750.4	3.897	0.001715	1663.3	1704.5	3.811	0.001581	1605.1	1660.1	3.713	0.001507	1568.4	1637.2	3.651	360
380	0.002749	1987.1	2052.8	4.35	0.002165	1867.2	1922	4.145	0.001805	1757.9	1816.6	3.962	0.001656	1698.3	1768.3	3.863	380
400	0.005284	2372.9	2510.3	5.03	0.002937	2093.3	2180.3	4.518	0.002102	1913.8	1987.5	4.213	0.001838	1829.3	1908.6	4.072	400
420	0.007579	2580	2769.4	5.42	0.004566	2371.7	2512.3	4.999	0.002518	2077.6	2174.1	4.475	0.002065	1962.6	2056.8	4.282	420
440	0.008697	2679.6	2897.1	5.601	0.006228	2562	2748.9	5.342	0.003138	2254.3	2381.2	4.761	0.002355	2099.8	2213.5	4.496	440
460	0.009617	2758.8	2999.2	5.743	0.007193	2668	2883.8	5.528	0.004149	2447.4	2613.3	5.084	0.002741	2242.4	2379.6	4.72	460
480	0.01042	2826.6	3087.1	5.861	0.007992	2752.2	2992	5.674	0.00495	2579.2	2777.2	5.305	0.003277	2391.7	2556.8	4.957	480
500	0.01114	2887.4	3165.9	5.964	0.00869	2824.1	3084.8	5.796	0.005625	2681.7	2906.7	5.475	0.003889	2528	2722.5	5.176	500
520	0.01181	2943.2	3238.5	6.057	0.00932	2888.1	3167.7	5.901	0.006213	2766.9	3015.4	5.613	0.004417	2636.5	2857.4	5.348	520
540	0.01244	2995.7	3306.6	6.142	0.009899	2946.7	3243.7	5.996	0.00674	2841.1	3110.7	5.732	0.004896	2728.4	2973.2	5.492	540
560	0.01303	3045.6	3371.3	6.22	0.01044	3001.6	3314.8	6.083	0.007221	2907.8	3196.7	5.837	0.005332	2808.8	3075.4	5.617	560
580	0.01359	3093.6	3433.5	6.294	0.01095	3053.6	3382.3	6.163	0.007669	2969.3	3276	5.931	0.005734	2881	3167.7	5.726	580
600	0.01414	3140.2	3493.7	6.364	0.01144	3103.5	3446.9	6.237	0.008089	3026.9	3350.4	6.017	0.006109	2947.2	3252.6	5.825	600
640	0.01518	3230.2	3609.7	6.494	0.01237	3198.9	3569.9	6.375	0.008869	3134.1	3488.8	6.172	0.006796	3067.4	3407.2	5.998	640
680	0.01617	3317.4	3721.5	6.614	0.01324	3290.1	3687.2	6.501	0.009589	3234	3617.6	6.31	0.007422	3176.9	3548	6.149	680
720	0.01711	3402.8	3830.6	6.726	0.01406	3378.6	3800.5	6.617	0.01026	3329.4	3740	6.436	0.008004	3279.5	3679.6	6.284	720
760	0.01803	3487.2	3937.9	6.832	0.01486	3465.5	3911.3	6.727	0.01091	3421.7	3857.9	6.552	0.008552	3377.4	3805	6.408	760
800	0.01892	3570.9	4044	6.932	0.01563	3551.4	4020.2	6.83	0.01152	3511.9	3972.8	6.661	0.009074	3472.3	3926	6.523	800

Table E.31: Supercritical steam (600 bar to 1000 bar)

$T(^{\circ}\text{C})$	600 bar				700 bar				800 bar				1000 bar				$T(^{\circ}\text{C})$
	v	u	h	s	v	u	h	s	v	u	h	s	v	u	h	s	
0.01	0.000972	0.2777	58.63	-0.00193	0.000968	0.1902	67.97	-0.00323	0.000964	0.0725	77.22	-0.00476	0.000957	-0.2439	95.43	-0.00844	0.01
20	0.000977	80.35	138.9	0.2818	0.000973	79.76	147.9	0.279	0.000969	79.19	156.7	0.2761	0.000962	78.04	174.2	0.27	20
40	0.000983	160.9	219.9	0.5489	0.00098	159.9	228.4	0.5449	0.000976	158.9	237	0.5409	0.000969	157	253.9	0.5329	40
60	0.000992	241.6	301.1	0.8004	0.000989	240.2	309.4	0.7955	0.000985	238.8	317.6	0.7905	0.000978	236.2	334	0.7808	60
80	0.001003	322.5	382.7	1.038	0.000999	320.7	390.6	1.032	0.000996	318.9	398.5	1.026	0.000988	315.5	414.4	1.015	80
100	0.001016	403.5	464.5	1.263	0.001012	401.3	472.1	1.257	0.001008	399.1	479.8	1.25	0.001	395	495	1.237	100
120	0.00103	484.8	546.7	1.478	0.001026	482.1	554	1.47	0.001022	479.5	561.3	1.463	0.001014	474.6	576	1.449	120
140	0.001047	566.5	629.3	1.683	0.001042	563.3	636.2	1.674	0.001037	560.2	643.2	1.666	0.001028	554.4	657.2	1.65	140
160	0.001065	648.5	712.4	1.879	0.00106	644.8	718.9	1.87	0.001054	641.2	725.5	1.861	0.001045	634.4	738.9	1.843	160
180	0.001085	731	796.2	2.068	0.001079	726.7	802.2	2.058	0.001074	722.5	808.4	2.048	0.001063	714.7	820.9	2.028	180
200	0.001108	814.2	880.7	2.251	0.001101	809.1	886.2	2.239	0.001095	804.3	891.8	2.228	0.001083	795.3	903.5	2.207	200
220	0.001133	898.2	966.2	2.428	0.001125	892.3	971	2.415	0.001118	886.7	976.1	2.402	0.001104	876.3	986.7	2.379	220
240	0.001161	983.2	1052.8	2.6	0.001152	976.3	1056.9	2.586	0.001143	969.8	1061.3	2.572	0.001128	957.9	1070.7	2.546	240
260	0.001193	1069.4	1141	2.769	0.001182	1061.4	1144.1	2.752	0.001172	1053.9	1147.7	2.737	0.001154	1040.2	1155.6	2.708	260
280	0.001229	1157.3	1231	2.934	0.001216	1147.8	1232.9	2.916	0.001204	1139.1	1235.4	2.898	0.001183	1123.3	1241.6	2.866	280
300	0.00127	1247	1323.3	3.098	0.001254	1235.9	1323.7	3.077	0.00124	1225.7	1324.9	3.057	0.001215	1207.4	1328.9	3.022	300
320	0.001318	1339.2	1418.3	3.261	0.001298	1325.9	1416.7	3.237	0.00128	1313.8	1416.3	3.214	0.00125	1292.7	1417.7	3.174	320
340	0.001374	1434.2	1516.7	3.424	0.001349	1418.1	1512.5	3.395	0.001327	1403.8	1509.9	3.369	0.00129	1379.1	1508.1	3.324	340
360	0.001457	1541.1	1623.1	3.604	0.001419	1519.1	1613.7	3.565	0.001388	1500.4	1607.4	3.532	0.001339	1469.6	1600.6	3.477	360
380	0.001569	1657.8	1740.6	3.794	0.001509	1627.2	1722.8	3.742	0.001464	1602.5	1710.7	3.7	0.001398	1563.5	1696.5	3.632	380
400	0.001701	1775.1	1864.6	3.982	0.001613	1735.6	1836.8	3.916	0.001549	1704.7	1818	3.863	0.001462	1657.5	1795.2	3.782	400
420	0.001856	1893.4	1994.1	4.167	0.001731	1844.5	1955	4.086	0.001645	1807.1	1928.5	4.023	0.001532	1751.3	1896	3.929	420
440	0.002042	2013.3	2126.8	4.352	0.001868	1954.2	2076.9	4.235	0.001754	1909.9	2041.9	4.181	0.001609	1845.1	1998.7	4.073	440
460	0.00227	2135.4	2268.6	4.539	0.002028	2065	2202.2	4.422	0.001877	2013.2	2158	4.337	0.001694	1939.1	2103.3	4.214	460
480	0.002555	2260.1	2413.7	4.73	0.002219	2177	2330.9	4.591	0.00202	2117.2	2276.4	4.492	0.001789	2033.2	2209.4	4.354	480
500	0.002922	2388	2564.6	4.926	0.002449	2290.5	2462.9	4.761	0.002186	2222	2397.1	4.647	0.001895	2127.6	2316.8	4.491	500
520	0.003361	2512.3	2713.9	5.119	0.002732	2405.5	2598.3	4.933	0.002382	2327.5	2519.8	4.801	0.002015	2222.1	2425.3	4.627	520
540	0.003762	2617.2	2842.9	5.28	0.003067	2518.7	2733.4	5.103	0.002616	2433.9	2644.8	4.957	0.00215	2316.8	2534.8	4.762	540
560	0.004142	2709.6	2958.1	5.42	0.003378	2617.6	2854.1	5.25	0.002885	2538.2	2769	5.11	0.002305	2411.7	2645.3	4.896	560
580	0.004499	2792.1	3062	5.543	0.003683	2707.3	2965.1	5.382	0.003135	2631.2	2882	5.244	0.002484	2506.8	2756.8	5.031	580
600	0.004834	2866.9	3157	5.653	0.003975	2789.3	3067.5	5.5	0.003384	2717.4	2988.1	5.367	0.002672	2597.8	2865.1	5.158	600
640	0.005447	3000.4	3327.3	5.844	0.00452	2934.8	3251.2	5.706	0.003861	2872.1	3181	5.583	0.003026	2761.2	3063.8	5.381	640
680	0.006003	3119.6	3479.8	6.007	0.005018	3063.1	3414.4	5.881	0.004306	3008.5	3352.9	5.768	0.003376	2907.7	3245.3	5.575	680
720	0.006518	3229.5	3620.6	6.152	0.005478	3180.2	3563.6	6.034	0.00472	3132.1	3509.7	5.929	0.003712	3041.7	3413	5.748	720
760	0.007	3333.2	3753.2	6.283	0.005909	3289.5	3703.1	6.172	0.005108	3246.7	3655.3	6.073	0.004031	3165.5	3568.6	5.901	760
800	0.007457	3432.7	3880.2	6.403	0.006317	3393.6	3835.8	6.298	0.005476	3355.2	3793.3	6.204	0.004336	3281.6	3715.2	6.04	800

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Perfect gas properties in Table E.3 are based on data from *Technical Data on Fuel* (7th edition), ed. J.W. Rose and J.R. Cooper, Scottish Academic Press, 1977.

Enthalpies of ideal (but not perfect) gases in Table E.5 are approximate values obtained from fitting quadratic relationships to enthalpy-temperature data from Rose and Cooper, *Technical Data on Fuel*; the coefficients of the corresponding linear specific heat relationships and the mean and maximum errors are also given. This allows a choice between tabular and analytical methods for solving combustion problems, with consistent results. The particular form of functional relationship is one, which enables combustion product temperature to be found without iteration. Tables E.8 and E.9, for heating (or calorific) values (negative of enthalpies of combustion) of simple compounds and some typical fuels, is based on data from the same source.

The Moody diagram of Figure E.1 was plotted using the equation of Colebrook and White for turbulent flow in rough pipes and Prandtl's equation for turbulent flow in smooth pipes, as quoted in Engineering Sciences Data Unit document ESDU 66027.

The psychrometric chart in Figure E.2, for standard atmospheric pressure, is based on that published in 1970 by the Institution of Heating and Ventilating Engineers.

The R134a data of Tables E.10 to E.15 have been condensed from much more detailed tables in the ICI Chemicals & Polymers Ltd publication *Thermodynamic Properties of KLEA134a*. Other physical properties of R134a, together with the equations from which the thermodynamic properties were computed, are in *Physical Property Data KLEA134a*, ICI Chemicals & Polymers Ltd, Runcorn, 1993. The refrigerants business ICI Klea was acquired in 2001 by INEOS Fluor.

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